

# **Department of Community Development** 922 Machin Avenue, Novato, CA 94945 Inspections: (415) 899-8240 Office: (415) 899-8989 Fax: (415) 899-8216 www.novato.org

**Building Division** PERMIT NUMBER

B2022-2111

Print Date: 10/31/2022

Paid at Issuance

DIF Balance Due at Final

Residential Development Impact Fees (DIF) Due Prior to Final

To obtain this permit, the undersigned hereby files this application and agrees, certifies, and declares: Notice has been given to me that this permit may be used only in compliance with the Novato Municipal Code and all other applicable ordinances and laws. This permit does not allow additional work to be performed. I agree to comply with all City and County ordinances and State laws relating to building construction and hereby authorize representative of the City of Novato permission to enter the job premises at any reasonable time to inspect any work installed under this permit and remove any nonconforming construction at my expense. Refunds made after 30 days but before 90 days from issuance of permit will be determined by the Building Official; No refunds after 90 days. (CDD/PW Fee Schedule, Item 16. Refund of Permit Fees.)

#### LICENSED CONTRACTOR'S DECLARATION

EICENSED CONTRACTOR'S DECLARATION				
I hereby affirm under penalty of perjury that I am licensed under provisions of Chapter 9				
(commencing with Section 7000) of Division 3 of the Business and Professions Code, and my license is in full force and effect.	1 1 1 1 1 1 1	10. 10. 1. 15	Cia Cia	
License Class C-10 Lic No. C:923979	Applied Date	Approved Date Issued I	The state of the s	
	08/25/2022	10/19/2022 10/31	/2022	
Exp. Date 10/31/2022 Contractor GENERAL DYNAMICS INFORMATION TECHNOL		Valuation	Lot	Subdivision
OWNER BUILDING DECLARATION		\$ 31,500.00	Loc	Subdivision
I hereby afirm under penalty of perjury that I am exempt from the Contractor's License Law for the following reason (Section 7031.5, Business and Professions Code: Any city	Job Site Address	1		APN
or county that requires a permit to construct, alter, improve, demolish, or repair any structure, prior to its issuance, also requires the applicant for the permit to file a signed	150 HAMILTO	N DR		157-171-17
statement that he or she is licensed pursuant to the provisions of the Contractors License Law (Chapter 9 (commencing with Section 7000) of Division 3 of the Business and Professions Code) or that he or she is exempt therefrom and the basis for the alleged exemption. Any violation of Section 7031.5 by any applicant for a permit subjects the applicant to a civil penalty of not more that five hundred dollars (\$500).):  I, as owner of the property, or my employees with wages as their sole compensation,	Owner NEW CINGULAR V 2700 WATTT AVEN	Contractor GENERAL DYNAMI 101 STATION DR #DO	05	
will do the work, and the structure is not intended or offered for sale (Section 7044, Business and Professions Code: The Contractor's License Law does not apply to an owner of property who builds or improves thereon, and who does the work himself or herself or through his or her own employees, provided that the improvements are not intended or offered for sale. If, however, the building or improvement is sold within one year of completion, the owner-builder will have the burden of proving that he or she did	SACRAMENTO Phone: (916) 715- Fax:	WESTWOOD Phone: (619) 402-84 Fax: License No. C:923979	MA 02090 90	
not build or improve for the purpose of sale.)	Lessee		Applicant	
I, as owner, of the property, am exclusively contracting with licensed contractors to construct the project (Section 7044, Business and Professions Code: The Contractor's License Law does not apply to an owner of property who builds or improves thereon and who contracts for the projects with a contractor(s) licensed pursuant to the Contractor's	Phone:		FRANK SCHABAI 10615 QUAIL HOI REDDING	
License Law.)	Fax:		REDDING	OA 90003
I am exempt under Sec, B&P.C for this reason	Description of Work			
WORKER'S COMPENSATION DECLARATIONS I hereby affirm under penalty of perjury one of the following declarations:  I have and will maintain a certificate of consent to self-insure for workers' compensation, as provided for by Section 3700 of the Labor Code, for the performance of the work for which this permit is issued.  I have and will maintain workers' compensation insurance, as required by Section 3700 of the Labor Code, for the performance of the work for which this permit is issued.  My workers' compensation insurance carrier and policy number are:	on new 9-2 x 15'-0 c concrete foundation.	30k/w standby diesel generator oncrete foundation. Install new Install new ATS and camlock, new fire extinguisher cabinet an	4'-0" X 9'-2" concrete sto PG&E generator docume	oop adjoing new ent box, fire
Carrier A I U INSURANCE				
Policy No. WC16393276 Expire: 7/1/2023				
I certify that, in the performance of the work for which this permit is issued, I shall	FEE D	ESCRIPTION AND F	EES [refer to receip	for details]
not employ any person in any manner so as to become subject to the workers' compensation laws of California, and agree that, if I should become subject to the workers' compensation provisions of Section 3700 of the Labor Code, I shall forthwith comply with those provisions.	GREEN	NG PERMIT FEES BUILDING STANDARDS TORAGE		\$466.70 \$2.00 \$3.90
WARNING: FAILURE TO SECURE WORKERS COMPENSATION COVERAGE IS UNLAWFUL, AND SHALL SUBJECT AN EMPLOYER TO CRIMINAL PENALTIES AND CIVIL FINES UP TO ONE HUNDRED THOUSAND DOLLARS (\$100,000), IN ADDITION TO THE COST OF COMPENSATION DAMAGES AS PROVIDED FOR IN SECTION 3706 OF THE LABOR CODE, INTEREST, AND ATTORNEYS FEES.	SURCHA PLAN C	ARGES HECK FEES		\$98.01 \$1,318.76
I certify that I have read this application and state that the above information is correct. I agree to comply with all city and county ordinances and state laws relating to building construction, and hereby authorize representatives of this City to enter upon the above-mentioned property for inspection purposes.				
I understand all work must be inspected and approved before placing concrete or concealing framing, electrical, plumbing, or mechanical work. A final inspection and certificate of occupancy must be obtained prior to occupancy and clearance for connection of utilities.				
Frank Schabarum 10/31/2022	1		Total Fee	s \$ 1,889.37
			Paid at Issuana	\$ 1,889.37

This permit will expire if work is not started in 180 days or if work is abandoned for more than 180 days.

DATE

SIGNATURE OF APPLICANT OR AGENT

# NONRESIDENTIAL INSPECT. REQ.

(INSPECTION REQUEST: 415-899-8240)

# **Inspection Record**

**Job Location 150 HAMILTON DR** 

**Job Description** Install new Generac 30k/w standby diesel generator with UL 2085 rated 190 gallon base fuel tank on new 9-2 x 15'-0 concrete foundation. Install new 4'-0" X 9'-2" concrete stoop adjoing new concrete foundation. Install new ATS and camlock, PG&E generator document box, fire extinguisher within new fire extinguisher cabinet and lockable emergency shutoff switch to side of existing and adjoining AT&T equipment shelter. Install new underground conduit and generator cable from generator location to new ATS.

Permit No. B2022-2111 Date Issued 10/31/2022

Owner NEW CINGULAR WIRELESS PCS, LLC dba AT&T MOBILITY

Type of Inspection	Date	Inspector	Type of Inspection	Date	Inspector
Site/Foundation IN	SPECTION	N CODE: 300	Energy and Sustainability INSPECTION CODE: 340		
			☐ Green Bldg. Components		
☐ Foundation Wall			☐ Green Bldg. Compliance		
☐ Foundation Drains			☐ Energy Compliance		
☐ Piers, Caissons					
□ Anchors			Gas Meter Authorization INSPECTION CODE: 370		
☐ Erosion Control			☐ Gas Test		
☐ Vaper Barrier			□ HVAC		
☐ Underfloor Venational			☐ Fireplace/Gas Insert		
Utilities IN:	SPECTION	N CODE: 310	Water Meter Authorization INSPECTION CODE: 380	l	
☐ Underfloor/Slab Elec			☐ Water Test		
☐ Underfloor/Slab Plg.			☐ Water Heater		
☐ Underfloor/SlabMech.			☐ Shower Pan		
Close In INS	 SPECTION	CODE: 320	Electric Meter Authorization INSPECTION CODE: 390	n	
☐ Rough Electrical			☐ Grounding Electrode (Ufer)		
☐ Rough Plumbing					
☐ Rough Mech.			Required form at Final Insp	pection	
☐ Hold Dn Brackets			☐ Energy Documentation		
			☐ Green Building		
8	<b>SPECTION</b>	CODE: 325			
☐ Roof Underlayment and Flashing			Required Final Approvals		
			FINAL APPROVALS INSE		
Wall Sheathing INS	<u>SPECTION</u>	CODE: 330	Final Approvals	Date	By
		1	☐ Building		
	SPECTION	N CODE: 335	☐ Planning		
☐ Fire Rated Assemblies			☐ Engineering		

#### **NOTICE**

It is the responsibility of the Permittee to:

- 1. Keep this inspection record/card and the approved plans on the job site for inspection.
- 2. Request inspections 24 hours in advance from the Building Division office for each stage of work. Each stage of work must be left exposed for inspection and approved before covering. Inspections can be scheduled by phoning the Automated Building Inspection Request Line: 899-8240. Every effort will be made to respond the following working day to all calls received. Due to the difficulty of scheduling inspections, no specific time for appointments can be assumed unless prior arrangements are made with the Building Inspector.
- 3. It is the responsibility of the owner to ensure compliance with any private deed restrictions or CC&R's, including any required architectural review.
- 4. It is your responsibility to coordinate final inspections with the appropriate agencies indicated by a checkmark on the "Inspection Record" and/or "Final Occupancy and Utility Approval" form. A "Final Occupancy and Utility Approval" and a release of utilities will not be granted by the Building Division until these spaces are signed by the required 24-48 hours advance notice for an inspection. Some, such as the Planning Division require submission of other forms and materials prior to performing the inspection.

**EXPIRATION**: This permit shall expire if there is more than 180 days without an inspection - permit valid for maximum of 2 years if inspections are made within 180 day time frames.

**NOTE:** When an extra inspection is required due to the job not being ready when an inspection is called for, or the approved plans are not available on the job, or when the inspector has no access to the project, a reinspection fee will be required. You should be ready for an approval before you call for an inspection. If you cannot keep an appointment, please cancel by phoning the Building Division. If you have any questions, please call the Building Division at 899-8989.

**WARNING:** If Final Inspection and approvals are not obtained the building permit will expire by limitation and the owner will be subject to enforcement action including additional permit fees, citation, and/or a nuisance abatement hearing before the City Council.

		☐ Fire District	
Miscellaneous	<b>INSPECTION CODE: 399</b>	☐ Sanitary District	
		□ NM Water District	
		□ NPD Crime Prevention	
		☐ MC Health Department	

#### Permit No. B2022-2111

<b>Type of Inspection</b>	Date	Inspector	Type of Inspection	Date	Inspector	Type of Inspection	Date	Inspector
Masonry INSPECTION CODE: 350		CODE: 350	Temporary Power INSPECTION CODE: 390			Special Inspections/Test Reports p	er special i	nspection &
Retaining Wall Footing			Overhead service			Testing agreement. Must be signed	d by special	
Steel Reinforcement			Underground service			Inspector <b>prior</b> to calling for City	inspection.	
1 <sup>st</sup> Lift			Electrical Service Uprade					
2 <sup>nd</sup> Lift			GFI Breakers			Soils compliance prior to		
3 <sup>rd</sup> Lift						foundation inspection.		
Fireplace Throat						3-Test cylinders		
Fireplace Top Out			ACCESSIBILITY INSPEC	CODE: 3	60 (Exterior)	Pier/caisson reinforcing		
Fireplace Seismic Straps			ACCESSIBILITY INSPEC	CODE: 3	65 (Interior)			
Stucco IN:	SPECTION	N CODE: 355	Entrance			Masonry/reinforcing		
Veneer			Path of travel			Structural concrete over		
Lathing			Sanitary facilities			2500 PSI by design		
Scratch Coat			Drinking fountain			Foundation reinforcing		
Brown Coat			Public phone			High strength bolts		
			Parking - other			Spayed on fire proofing		
Suspended Ceiling INS	SPECTION	I CODE: 345				Retaining walls backfill/drains		
T Bar Ceiling			INFORMATIONAL/STAT	US INSPE	C CODE: 399			
T Bar Cross Bracing			Miscellaneous					
Fixture Supports								

Full Job Description: Install new Generac 30k/w standby diesel generator with UL 2085 rated 190 gallon base fuel tank on new 9-2 x 15'-0 concrete foundation. Install new 4'-0" X 9'-2" concrete stoop adjoing new concrete foundation. Install new ATS and camlock, PG&E generator document box, fire extinguisher within new fire extinguisher cabinet and lockable emergency shutoff switch to side of existing and adjoining AT&T equipment shelter. Install new underground conduit and generator cable from generator location to new ATS.

Inspector's Comments:	
	CITY OF NO 922 Machin A Novato, CA

**OVATO** Avenue 94945

THE CITY OF NOVATO CALIFORNIA



# Transaction Receipt from City of Novato for \$1889.37 (USD)

Auto-Receipt <noreply@mail.authorize.net> Reply-To: Trevor Alton <talton@novato.org>

To: Frank Schabarum <frank.schabarum123@gmail.com>

Mon, Oct 31, 2022 at 1:01 PM

Order Information

Description: Goods or Services

Invoice Number 20221031125825 PO Number WEB12218

**Billing Information** 

**Shipping Information** 

Frank Schabarum

Frank Schabarum

General Dynamics Information Technology, Inc General Dynamics Information Technology, Inc

10615 Quail Hollow Drive

10615 Quail Hollow Drive

Redding, CA 96003

Redding, CA 96003

**United States** 

**United States** 

frank.schabarum123@gmail.com

6197430309

Total: \$1889.37 (USD)

Payment Information

Date/Time: 31-Oct-2022 13:01:08 PDT

Transaction ID: 64023506098 Payment Method: Visa xxxx8063 Transaction Type: Purchase Auth Code: 52185D

Merchant Contact Information

City of Novato Novato, CA 94945

US

talton@novato.org

SITE INFORMATION:

SITE ADDRESS:

COORDINATES:

PROPERTY LANDLORD

OCCUPANCY GROUP:

CONSTRUCTION TYPE:

POWER COMPANY:

A.D.A. COMPLIANCE:

DO NOT SCALE DRAWINGS:

CONTACT INFORMATION:

FLOOD ZONE:

APPLICANT

PROJECT MANAGER:

LEASING / PERMITTING:

ARCHITECTURE &

ENGINEERING

COUNTY:

OR OWNER

TAX ID #

ZONING:

150 HAMILTON ROAD

38.0782481° / -122.5415981° (FOR NAVIGATION ONLY)

NOVATO, CA 94945

PG&F

C1-1

II-B

PG&E

157-171-17

U - UNMANNED

AE (EL = 10FT AMSL NAVD88)

CONTRACTOR SHALL VERIFY ALL PLANS, EXISTING DIMENSIONS, CONDITIONS ON

THE JOB SITE AND SHALL IMMEDIATELY NOTIFY THE ENGINEER IN WRITING OF ANY

DISCREPANCIES BEFORE PROCEEDING WITH THE WORK OR BE RESPONSIBLE FOR

1375 CAMINO REAL STE 120

SAN BERNARDINO, CA 92408

AT&T MORILITY

PHONE: 951 534 8967

SEA TAC, WA 98048

PHONE: 425.606.8785

JT LAND MANAGEMENT

REDDING, CA 96003

PHONE: 530.722.0743

PO BOX 2621

**BOISE ID 83701** 

GEOSTRUCTURAL, LLC.

PHONE: 530.539.4787

CONTACT: DON GEORGE

10615 QUAIL HOLLOW LANE

CONTACT: FRANK SCHABARUM

FACILITY IS UNMANNED AND NOT FOR HUMAN

GENERAL DYNAMICS WIRELESS SERVICES, LLC.

19240 DES MOINES DR. S. BLDG C STE 300

CONTACT: CHRISTOPHER HERMAN

# y eceine! By: Julie Williams

CITY OF NOVATO

**HWY 101 - IGNACIO** FA#: 10088152

LINE NAME: FULTON-IGNACIO #1 230KV

TOWER NUMBER: 40/192

SAP TOWER#: 40663880

GENERATOR INSTALLATION PROJECT

**30KW GENERAC DIESEL GENERATOR** 

WITH ASSOCIATED UL-2085 FUEL TANK

**150 HAMILTON ROAD** 

**NOVATO, CA 94945** 

CODE COMPLIANCE:

CALIFORNIA BUILDING CODE (CBC) 2019

CALIFORNIA ELECTRICAL CODE 2019

CALIFORNIA MECHANICAL CODE 2019

INTERNATIONAL BUILDING CODE (IBC) 2018

NATIONAL ELECTRICAL CODE (NEC) 2017

AMERICAN CONCRETE INSTITUTE (ACI) 318

AMERICAN INSTITUTE OF STEEL CONSTRUCTION (AISC)

TELECOMMUNICATIONS INDUSTRY ASSOCIATION (TIA) 222

TELECOMMUNICATIONS INDUSTRY ASSOCIATION (TIA) 607

DESCRIPTION

TITLE SHEET

**GENERAL NOTES** 

PARCEL SITE PLAN

**OVERALL SITE PLAN** 

**ENLARGED SITE PLAN** 

GENERATOR PAD DETAILS

FENCE & GATE DETAILS

GRADE BUILD-UP DETAIL

ELECTRICAL DETAILS

**ELECTRICAL DETAILS** 

**ELECTRICAL DETAILS** 

ATS SPECIFICATIONS

GENERATOR SPECIFICATIONS

CAM-LOCK BOX SPECIFICATIONS

GENERAL STRUCTURAL DETAILS

COMPOUND EXPANSION DETAIL

**ELEVATION VIEWS** 

CALIFORNIA FIRE CODE (CFC) 2019

SHEET INDEX:

ALL WORK AND MATERIALS SHALL BE PERFORMED AND INSTALLED IN

ADOPTED BY THE LOCAL GOVERNING AUTHORITIES. NOTHING IN THESE

PLANS ARE TO BE CONSTRUCTED TO PERMIT WORK NOT CONFORMING TO

NATIONAL FIRE PROTECTION ASSOCIATION (NFPA) 13,30,37,58,70,72,110,111

ACCORDANCE WITH THE CURRENT EDITIONS OF ALL GOVERNING CODES AS

**CITY OF NOVATO** 

**GENERAL DYNAMICS** 



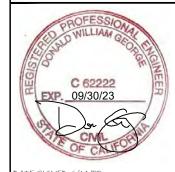
Information Technology

CONTACT@GEOSTRUCTURAL.COM WWW.GEOSTRUCTURAL.COM

	REVISIONS				
REV	DATE	DESCRIPTION	INT		
2	06/14/22	PGE GG	JAD		
1	02/15/22	PGE REDLINES	JAD		
0	01/05/22	ISSUED FOR CONSTRUCTION	KS		

CHECKED BY:

THE INFORMATION CONTAINED IN THIS SET OF THE INFORMATION CONTINUED IN THIS SET OF DOCUMENTS IS PROPRIETARY BY NATURE. ANY USE OR DISCLOSURE OTHER THAN THAT WHICH RELATES TO THE CLIENT NAMES IS STRICTLY PROHIBITED.



SITE INFORMATION:

HWY 101 - IGNACIO

10088152

GENERATOR INSTALLATION **PROJECT** 

> 150 HAMILTON ROAD NOVATO, CA 94945

JURISDICTION USE

#### **CITY OF NOVATO APPROVED**

PERMIT NO: B2022-2111 DATE: 10/19/2022

STAFF: Brian Macpherson

SHEET TITLE:

TITLE SHEET

SHEET NUMBER: T-1

JOB COPY



VICINITY MAP:

PLAN REVIEW ACCEPTANCE BY PHILLIPS SEABROOK ASSOCIATES APPLIES ONLY TO PLAN SHEETS WHICH HAVE THIS STAMP

# AREA MAP



# SITE

# APPROVALS AT&T MANAGER

GOOGLE MAPS 2021

# CONSTRUCTION MANAGER SITE ACQ. MANAGER PROPERTY LANDLORD

#### SCOPE OF WORK:

(GENERAC SD030) WITH UL-2085 BASE FUEL TANK ON CONCRETE PAD WITHIN NEW COMPOUND AND 200A ATS / CAMLOCK (GENERAC TAS200) NEAR EXISTING AT&T EQUIPMENT AREA. INSTALL NÈW GEN DOCS BOX INSIDE FENCED AREA

GROUND STRUCTURES, AND/OR EXISTING UTILITIES BELIEVED TO BE IN THE WORKING AREA. IT IS THE RESPONSIBILITY OF THE CONTRACTOR TO VERIFY ALL UTILITIES, PIPELINES AND OTHER STRUCTURES SHOWN OR NOT SHOWN ON THESE PLANS

UTILITIES SHALL BE REPAIRED TO THE SATISFACTION OF THE OWNER AND ENGINEER AT THE CONTRACTOR'S EXPENSE



INSTALL (1) ARTICLE 702 OPTIONAL STANDBY DIESEL GENERATOR

INTEGRATE NEW GENERATOR WITH EXISTING SERVICE NOTE: NO CHANGES OR ALTERATIONS TO THE TOWER, MOUNTS, ANTENNAS, FEEDLINES, ETC. IS PROPOSED AS A PART OF THIS SCOPE OF WORK

THE PLANS SHOW SOME KNOWN SUBSURFACE STRUCTURES, ABOVE

ANY DAMAGE TO EXISTING

A-0 A-2 S-2

> S-3 S-4.1

> > E-5.0

E-5.1

F-3 0 E-3.1, E-3.2, E-3.3 PG&E GROUNDING SPECIFICATIONS F-4 0 <> F4 4

#### NOTES TO SUBCONTRACTOR:

- THE GENERAL SUBCONTRACTOR MUST VERIFY ALL DIMENSIONS, CONDITIONS AND ELEVATIONS BEFORE PROCEEDING WITH THE WORK. ALL DISCREPANCIES SHALL BE RESOLVED BEFORE PROCEEDING WITH THE WORK. ALL WORK SHALL BE PERFORMED IN A WORKMANLIKE MANNER IN ACCORDANCE WITH ACCEPTED CONSTRUCTION PRACTICES.
- 2. IT IS THE INTENTION OF THESE DRAWINGS TO SHOW THE COMPLETED INSTALLATION. THE SUBCONTRACTOR SHALL BE RESPONSIBLE FOR ALL TEMPORARY BRACING, SHORING, TIES, FORM WORK, ETC. IN ACCORDANCE WITH ALL NATIONAL, STATE, AND LOCAL ORDINANCES, TO SAFELY EXECUTE ALL WORK AND SHALL BE RESPONSIBLE FOR SAME. ALL WORK SHALL BE IN ACCORDANCE WITH LOCAL CODES.
- 3. THE SUBCONTRACTOR SHALL USE ADEQUATE NUMBER OF SKILLED WORKMAN WHO ARE THOROUGHLY TRAINED AND EXPERIENCED IN THE NECESSARY CRAFTS AND WHO ARE COMPLETELY FAMILIAR WITH THE SPECIFIED REQUIREMENTS AND METHOD NEEDED FOR PROPER PERFORMANCE
- 4. SUBCONTRACTOR AGREES THAT IN ACCORDANCE WITH GENERALLY ACCEPTED CONSTRUCTION PRACTICES. CONSTRUCTION SUBCONTRACTOR WILL BE REQUIRED TO ASSUME SOLE AND COMPLETE RESPONSIBILITY FOR JOB SITE CONDITIONS DURING THE COURSE OF CONSTRUCTION OF THE PROJECT, INCLUDING THE SAFETY OF ALL PERSONS AND PROPERTY, THAT THIS REQUIREMENT SHALL BE MADE TO APPLY CONTINUOUSLY AND NOT BE LIMITED TO NORMAL WORKING HOURS AND SUBCONTRACTOR FURTHER AGREES TO INDEMNIFY AND HOLD DESIGN ENGINEER HARMLESS FROM ANY AND ALL LIABILITY, REAL OR ALLEGED, IN CONNECTION WITH PERFORMANCE OF WORK ON THIS
- 5. SITE GROUNDING SHALL COMPLY WITH AT&T WIRELESS SERVICES TECHNICAL SPECIFICATIONS FOR FACILITY GROUNDING FOR CELL SITE STANDARDS, LATEST EDITION, AND COMPLY WITH AT&T TOWERS GROUNDING CHECKLIST, LATEST VERSION. WHEN NATIONAL AND LOCAL GROUNDING CODES ARE MORE STRINGENT THEY SHALL GOVERN.
- 6. ALL WORK SHALL COMPLY WITH OSHA AND STATE SAFETY REQUIREMENTS. PROCEDURES FOR THE PROTECTION OF EXCAVATIONS, EXISTING CONSTRUCTION AND UTILITIES SHALL BE ESTABLISHED PRIOR TO FOUNDATION INSTALLATION.
- 7. ALL WORK SHALL BE ACCOMPLISHED IN ACCORDANCE WITH ALL LOCAL, STATE, AND FEDERAL CODES OR ORDINANCES. THE MOST STRINGENT CODE WILL APPLY IN THE CASE OF DISCREPANCIES OR DIFFERENCES IN THE CODE REQUIREMENTS
- 8. ANY DAMAGE TO THE ADJACENT PROPERTIES WILL BE CORRECTED AT THE SUBCONTRACTOR'S EXPENSE TO THE SATISFACTION OF THE LANDOWNER AND THE CONSTRUCTION MANAGER.
- 9 THE COMPLETE BID PACKAGE INCLUDES THESE CONSTRUCTION DRAWINGS ALONG WITH THE SPECIFICATIONS. SUBCONTRACTOR IS RESPONSIBLE FOR REVIEW OF TOTAL BID PACKAGE PRIOR TO BID SUBMITTAL
- 10. SUBCONTRACTOR SHALL VERIFY LOCATION OF ALL EXISTING UTILITIES WITHIN CONSTRUCTION LIMITS PRIOR TO CONSTRUCTION.
- 11. THE SUBCONTRACTOR IS RESPONSIBLE FOR MAINTAINING POSITIVE DRAINAGE ON THE SITE AT ALL TIMES. SILT AND EROSION CONTROL SHALL BE MAINTAINED ON THE DOWNSTREAM SIDE OF THE SITE AT ALL TIMES. ANY DAMAGE TO ADJACENT PROPERTIES WILL BE CORRECTED AT THE
- 12. CLEARING OF TREES AND VEGETATION ON THE SITE SHOULD BE HELD TO A MINIMUM. ONLY THE TREES NECESSARY FOR CONSTRUCTION OF THE FACILITIES SHALL BE REMOVED. ANY DAMAGE TO THE PROPERTY OUTSIDE THE LEASED PROPERTY SHALL BE REPAIRED BY THE SUBCONTRACTOR
- 13. ALL SUITABLE BORROW MATERIAL FOR BACK FILL OF THE SITE SHALL BE INCLUDED IN THE BID. EXCESS TOPSOIL AND UNSUITABLE MATERIAL SHALL BE DISPOSED OF OFF SITE AT LOCATIONS APPROVED BY GOVERNING AGENCIES PRIOR TO DISPOSAL.
- 14. PERMITS: THE SUBCONTRACTOR SHALL BE RESPONSIBLE FOR OBTAINING AND INCURRING THE COST OF ALL REQUIRED PERMITS, INSPECTIONS, CERTIFICATES, ETC.
- 15. RECORD DRAWINGS: MAINTAIN A RECORD OF ALL CHANGES, SUBSTITUTIONS BETWEEN WORK AS SPECIFIED AND INSTALLED. RECORD CHANGES ON A CLEAN SET OF CONTRACT DRAWINGS WHICH SHALL BE TURNED OVER TO THE CONSTRUCTION MANAGER UPON COMPLETION
- 16. THE PLANS SHOW SOME KNOWN SUBSURFACE STRUCTURES. ABOVE GROUND STRUCTURES AND/OR EXISTING UTILITIES BELIEVED TO BE IN THE WORKING AREA. IT IS THE RESPONSIBILITY OF THE SUBCONTRACTOR TO VERIFY ALL UTILITIES, PIPELINES AND OTHER STRUCTURES SHOWN OR NOT SHOWN ON THESE PLANS. THE SUBCONTRACTOR SHALL CONTACT THE LOCAL LOCATE SERVICE BEFORE DIGGING OR DRILLING. ANY DAMAGE TO EXISTING UTILITIES SHALL BE REPAIRED TO THE SATISFACTION OF THE OWNER AND ENGINEER AT THE SUBCONTRACTOR'S EXPENSE.

#### REQUIRED SPECIAL INSPECTIONS:

1, PER CBC 1705.4 SPECIAL INSPECTION OF MASONRY, (IF REQUIRED)

PLAN REVIEW ACCEPTANCE BY PHILLIPS SEABROOK ASSOCIATES APPLIES ONLY TO PLAN SHEETS WHICH HAVE THIS STAMP

#### **GENERAL PROJECT NOTES:**

- THIS PROPOSAL IS FOR THE ADDITION OF A NEW GENERATOR ON A NEW CONCRETE PAD TO AN EXISTING UNMANNED TELECOMMUNICATIONS FACILITY CONSISTING OF AN EQUIPMENT SHELTER/PLATFORM AND TOWER.
- 2. THE PROPOSED FACILITY WILL BE UNMANNED AND DOES NOT REQUIRE POTABLE WATER OR
- 3. THE PROPOSED FACILITY IS UNMANNED AND IS NOT FOR HUMAN HABITAT. (NO HANDICAP
- I. OCCUPANCY IS LIMITED TO PERIODIC MAINTENANCE AND INSPECTION, APPROXIMATELY 2 TIMES PER MONTH BY AT&T TECHNICIANS.
- 5. OUTDOOR STORAGE AND SOLID WASTE CONTAINERS ARE NOT PROPOSED.
- 6. ALL MATERIAL SHALL BE FURNISHED AND WORK SHALL BE PERFORMED IN ACCORDANCE WITH THE PROJECT SPECIFICATIONS.
- 7. SUBCONTRACTOR SHALL BE RESPONSIBLE FOR REPAIRING ANY DAMAGE CAUSED BY THE CONSTRUCTION OPERATION
- 8. SUBCONTRACTOR SHALL BE RESPONSIBLE FOR OBTAINING ALL PERMITS AND INSPECTION
- 9. SUBCONTRACTOR SHALL REMOVE ALL TRASH AND DEBRIS FROM THE SITE ON A DAILY BASIS.

#### **ELECTRICAL NOTES:**

#### A. GENERAL

- . COORDINATE LOCATION AND POWER REQUIREMENTS OF ALL EQUIPMENT WITH AT&T AND EQUIPMENT SUPPLIER PRIOR TO INSTALLATION.
- 2. COORDINATE LOCATION AND REQUIREMENTS FOR ELECTRICAL AND TELEPHONE SERVICES WITH THE PROPERTY REPRESENTATIVE, AT&T AND UTILITY COMPANIES. ROUTING OF CONDUITS MAY BE MODIFIED TO MEET SITE REQUIREMENTS. EXACT CONDUIT ROUTING TO BE DETERMINED IN THE FIELD.
- 3. ALL WIRING AND EQUIPMENT SHOWN ON ELECTRICAL SHEETS SHALL BE FURNISHED AND INSTALLED UNDER ELECTRICAL PORTION OF CONTRACT UNLESS OTHERWISE NOTED
- 4. UNINTERRUPTED ELECTRICAL SERVICE FOR EXISTING EQUIPMENT SHALL BE MAINTAINED DURING THE INSTALLATION OF THE WORK DESCRIBED UNDER THESE DOCUMENTS. TEMPORARY EQUIPMENT, CABLES AND WHATEVER ELSE IS NECESSARY SHALL BE PROVIDED AS REQUIRED TO MAINTAIN ELECTRICAL SERVICE, TEMPORARY SERVICE FACILITIES, IF REQUIRED AT ANY TIME, SHALL NOT BE DISCONNECTED OR REMOVED UNTIL NEW SERVICE EQUIPMENT IS IN PROPER OPERATION. IF ANY SERVICE OR SYSTEM MUST BE INTERRUPTED, THE CONTRACTOR SHALL REQUEST PERMISSION IN WRITING STATING THE DATE, TIME, ETC. THE SERVICE WILL BE INTERRUPTED AND THE AREAS AFFECTED. THIS REQUEST SHALL BE MADE IN SUFFICIENT TIME FOR PROPER ARRANGEMENTS TO BE MADE. WRITTEN PERMISSION SHALL BE OBTAINED FROM THE OWNER BEFORE INTERRUPTING ELECTRICAL
- 5. COORDINATE NEW WORK WITH OTHER TRADES AND VERIFY EXISTING CONDITIONS TO AVOID INTERFERENCE. IN CASE OF INTERFERENCE, AT&T'S REPRESENTATIVE WILL DECIDE WHICH WORK IS TO BE RELOCATED, REGARDLESS OF WHICH WAS FIRST INSTALLED.
- 6. THE INSTALLATION MUST COMPLY WITH CEC AND ALL FEDERAL, STATE AND LOCAL RULES AND REGULATIONS.
- 7. THE DRAWINGS ARE DIAGRAMMATIC AND INDICATE THE GENERAL ARRANGEMENT OF SYSTEMS AND EQUIPMENT UNLESS OTHERWISE DEFINED BY DIMENSIONS OR DETAILS. EXACT EQUIPMENT LOCATIONS AND RACEWAY ROUTING SHALL BE GOVERNED BY ACTUAL FIELD CONDITIONS AND/OR DIRECTIONS FROM AT&T'S REPRESENTATIVE.
- 8. CONTRACTOR SHALL PAY ALL PERMITS AND FEES REQUIRED
- 9. ALL MATERIALS SHALL BE FURNISHED AND WORK SHALL BE PERFORMED IN ACCORDANCE WITH THE APPLICABLE SECTIONS OF THE STANDARDS REFERENCED BELOW:
- a. ANSI (AMERICAN NATIONAL STANDARDS INSTITUTE)
- b. ASTIM (AMERICAN SOCIETY FOR TESTING MATERIALS)
- c. ETL (ELECTRICAL TESTING LABORATORY)
- d. ICEA (INSULATED CABLE ENGINEERS ASSOCIATION)
- e. IEEE (INSTITUTE OF ELECTRICAL AND ELECTRONIC ENGINEERS) f MBFU (NATIONAL BOARD OF FIRE UNDERWRITERS)
- g. NESC (NATIONAL ELECTRICAL SAFETY CODE)
- h. NEMA (NATIONAL ELECTRICAL MANUFACTURER'S ASSOCIATION)
- i. NFPA (NATIONAL FIRE PROTECTION ASSOCIATION)
- j. UL (UNDERWRITER'S LABORATORY)
- k. NEC (NATIONAL ELECTRICAL CODE
- I. CEC (CALIFORNIA ELECTRICAL CODE)
- 10. CONTRACTOR SHALL REVIEW PLANS, DETAILS AND SPECIFICATIONS IN DETAIL AND ADJUST WORK TO CONFORM WITH ACTUAL SITE CONDITIONS SO THAT FLECTRICAL DEVICES AND EQUIPMENT WILL BE LOCATED AND READILY ACCESSIBLE. QUANTITIES LISTED IN MATERIAL LISTS ON THE DRAWINGS ARE FOR INFORMATION ONLY. THE CONTRACTOR SHALL PROVIDE HIS OWN TAKEOFF FOR MATERIAL QUANTITY AND TYPES BASED ON ACTUAL SITE CONDITIONS, IN ADDITION, CONTRACTOR SHALL PROVIDE ALL NECESSARY MATERIALS TO INSTALL EQUIPMENT FURNISHED BY AT&T OR ITS SUPPLIERS. ALL ITEMS NOT SPECIFICALLY MENTIONED HEREIN OR SHOWN ON THE DRAWINGS. BUT WHICH ARE OBVIOUSLY NECESSARY TO MAKE A COMPLETE WORKING INSTALLATION, SHALL BE INCLUDED
- 1. THE CONTRACTOR OR BIDDER SHALL BEAR THE RESPONSIBILITY OF NOTIFYING (IN WRITING) AT&T'S REPRESENTATIVE OF ANY CONFLICTS PRIOR TO THE SUBMISSION OF CONTRACTOR'S PROPOSAL OR PERFORMANCE OF WORK, IN THE EVENT OF DISCREPANCIES THE CONTRACTOR SHALL PRICE THE MORE COSTLY OR EXTENSIVE WORK, UNLESS DIRECTED IN WRITING OTHERWISE.

#### **ELECTRICAL NOTES:**

12. ALL FLOORS WHERE PENETRATIONS ARE REQUIRED IN BUILDING ARE TO BE CORE DRILLED

#### B. WIRING/CONDUIT

- PROVIDE PULL BOXES AND JUNCTION BOXES WHERE SHOWN OR AS REQUIRED BY CODE SUCH THAT NO MORE THAN THE EQUIVALENT OF FOUR QUARTER BENDS (360 DEGREES TOTAL) EXIST IN A CONDUIT RUN.
- 2. ALL POWER AND CONTROL/INDICATION WIRING SHALL BE TYPE THHN/THWN 600V RATED 75 DEGREES CELSIUS, UNLESS NOTED OTHERWISE.
- 3. CONDUIT BENDS SHALL BE MADE IN ACCORDANCE WITH NEC TABLE 346-10. NO RIGHT ANGLE DEVICE OTHER THAN STANDARD CONDUIT ELBOWS WITH 12" MINIMUM INSIDE SWEEPS FOR ALL CONDUITS 2" OR LARGER.
- 4. POWER WIRING SIZE SHALL NOT BE SMALLER THAN #12 AWG.
- 5. ALL WIRING SHALL BE COPPER. ALUMINUM WILL NOT BE ACCEPTABLE ALL POWER CIRCUITS SHALL CONTAIN A GROUND WIRE
- 6. PHASE MARKINGS TO BE USED AT POWER CONDUCTOR TERMINATIONS.
- 7. CONTRACTOR SHALL ENSURE INTEGRITY IS MAINTAINED WHEN INSTALLING CONDUIT AND
- 8. INSTALL PULL STRING IN ALL CONDUIT.
- ). FOR ROOFTOP INSTALLS AND BUILD-OUTS, CONDUITS INSIDE BUILDING AND ON ROOF SHALL BE RGS, UNLESS OTHERWISE NOTED. FOR RAW LAND SITES AND CO-LOCATES, PVC SCHEDULE 80 SHALL BE UTILIZED UNLESS NOTED OTHERWISE.
- 10. MAINTAIN MINIMUM 1'-0" VERTICAL AND 1'-0" HORIZONTAL SEPARATIONS FROM ANY MECHANICAL GAS PIPING.
- 11. ALL WIRING ROUTED IN PLENUM TO BE RATED OR IN METALLIC FLEX (LIQUIDTITE) CONDUIT.

- 1. EQUIPMENT/PARTS CONNECTED TO EXISTING PANELS, DUCTS, ETC. SHALL MATCH THE CHARACTERISTICS (A/C, V, A) OF THAT EQUIPMENT.
- 2. ALL ELECTRICAL EQUIPMENT OUTSIDE SHALL BE NEMA 3R RATED.

- 1. ALL GROUND CONNECTIONS TO BUILDING SHALL BE MADE USING TWO-HOLE CONNECTORS. PROVIDE STAINLESS STEEL BOLTS AND LOCK WASHERS ON ALL MECHANICAL GROUND
- 2. ALL EQUIPMENT SURFACES TO BE BONDED TO GROUNDING SYSTEM SHALL BE STRIPPED OF ALL PAINT AND DIRT AT ANY POINT OF CONNECTION. CONNECTIONS TO VARIOUS METALS SHALL BE OF A TYPE AS TO PREVENT A GALVANIC OR CORROSIVE REACTION. AREA SHALL BE REPAINTED FOLLOWING BONDING.
- 3. ANY METALLIC ITEM WITHIN 6' OF ANY EQUIPMENT OR METALLIC INFRASTRUCTURE (RACKS, CABLE TRAY.. ETC.) OR GROUND CONDUCTORS MUST BE CONNECTED TO THE
- 4. EXTERIOR, ABOVE GRADE GROUND CONNECTIONS SHALL BE FURNISHED WITH A LIBERAL PROTECTIVE COATING OF ANTI-OXIDATION COMPOUND.
- 5 ALL MATERIALS AND LABOR REQUIRED FOR THE GROUNDING SYSTEM AS INDICATED ON THE PLANS AND DETAILS, AND AS DESCRIBED HEREIN SHALL BE FURNISHED BY THE CONTRACTOR UNLESS OTHERWISE NOTED.
- 6. EXACT LOCATION OF GROUND CONNECTION POINTS SHALL BE DETERMINED IN FIELD. ADJUST LOCATIONS INDICATED ON PLANS ACCORDING TO ACTUAL EQUIPMENT LOCATIONS TO KEEP THE GROUND CONNECTION CABLES AS SHORT AND STRAIGHT AS PRACTICAL
- 7. PROVIDE ALL ELECTRICAL SYSTEM AND EQUIPMENT GROUNDS AS REQUIRED BY THE CURRENT EDITION OF THE NATIONAL ELECTRIC CODE, THE CURRENT EDITION OF THE NATIONAL ELECTRICAL SAFETY CODE AND AT&T STANDARDS. BONDING JUMPERS WITH APPROVED GROUND FITTINGS SHALL BE INSTALLED AT ALL RACEWAYS, EQUIPMENT ENCLOSURES, PULL BOXES, ETC. TO MAINTAIN GROUND CONTINUITY WHERE REQUIRED BY CODE.
- 8. ALL BURIED EQUIPMENT GROUND CONDUCTORS SHALL BE #2 AWG BARE, TINNED, SOLID COPPER UNLESS NOTED OTHERWISE ON THE DRAWINGS.

#### E. INSPECTION/DOCUMENTATION

- . THE CONTRACTOR, UPON COMPLETION OF HIS WORK, SHALL PROVIDE AS-BUILT DRAWINGS. INFORMATION SHOULD BE GIVEN TO THE GENERAL CONTRACTOR FOR INCLUSION IN FINAL AS-BUILT SURVEY DOCUMENTS TO BE GIVEN TO THE OWNER.
- 2. CONTRACTOR SHALL SUPPLY DOCUMENTATION ATTESTING TO THE COMPLETE GROUND SYSTEM'S RESISTANCE TO GROUND (MAX. 5 OHMS).
- 3. AN ELECTRICAL INSPECTION SHALL BE MADE BY AN INSPECTING AGENCY APPROVED BY AT&T'S REPRESENTATIVE. CONTRACTOR SHALL COORDINATE ALL INSPECTIONS AND OBTAIN POWER COMPANY APPROVAL
- 4. CONTRACTOR SHALL HAVE ATS AND GENERATOR RELAY INSTALLATION AND CONNECTIONS INSPECTED BY OTHERS TO ENSURE THAT ULLISTING FOR THAT EQUIPMENT IS NOT VOIDED.



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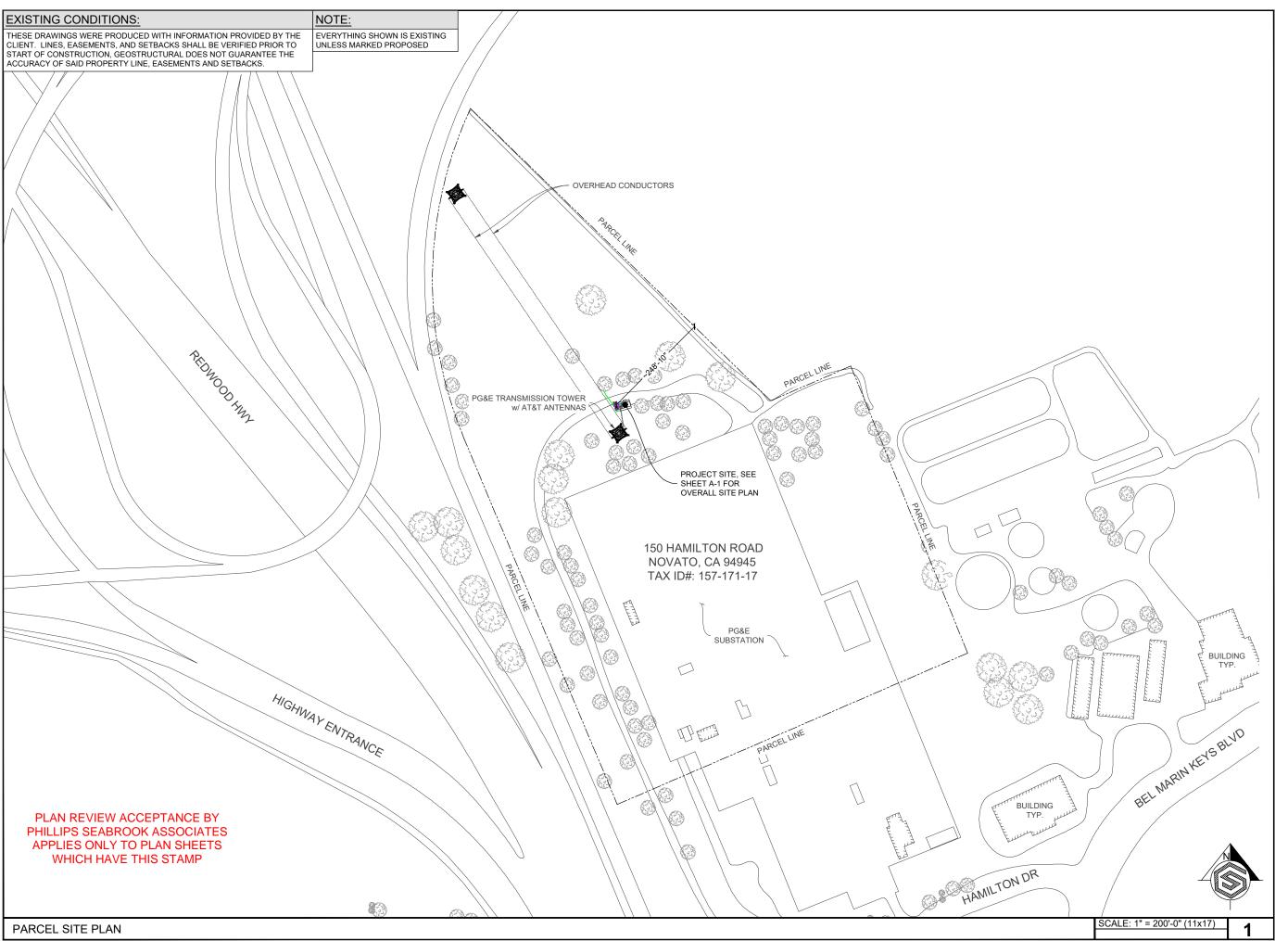
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**GENERAL NOTES** 

SHEET NUMBER





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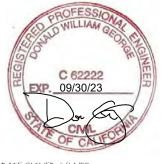
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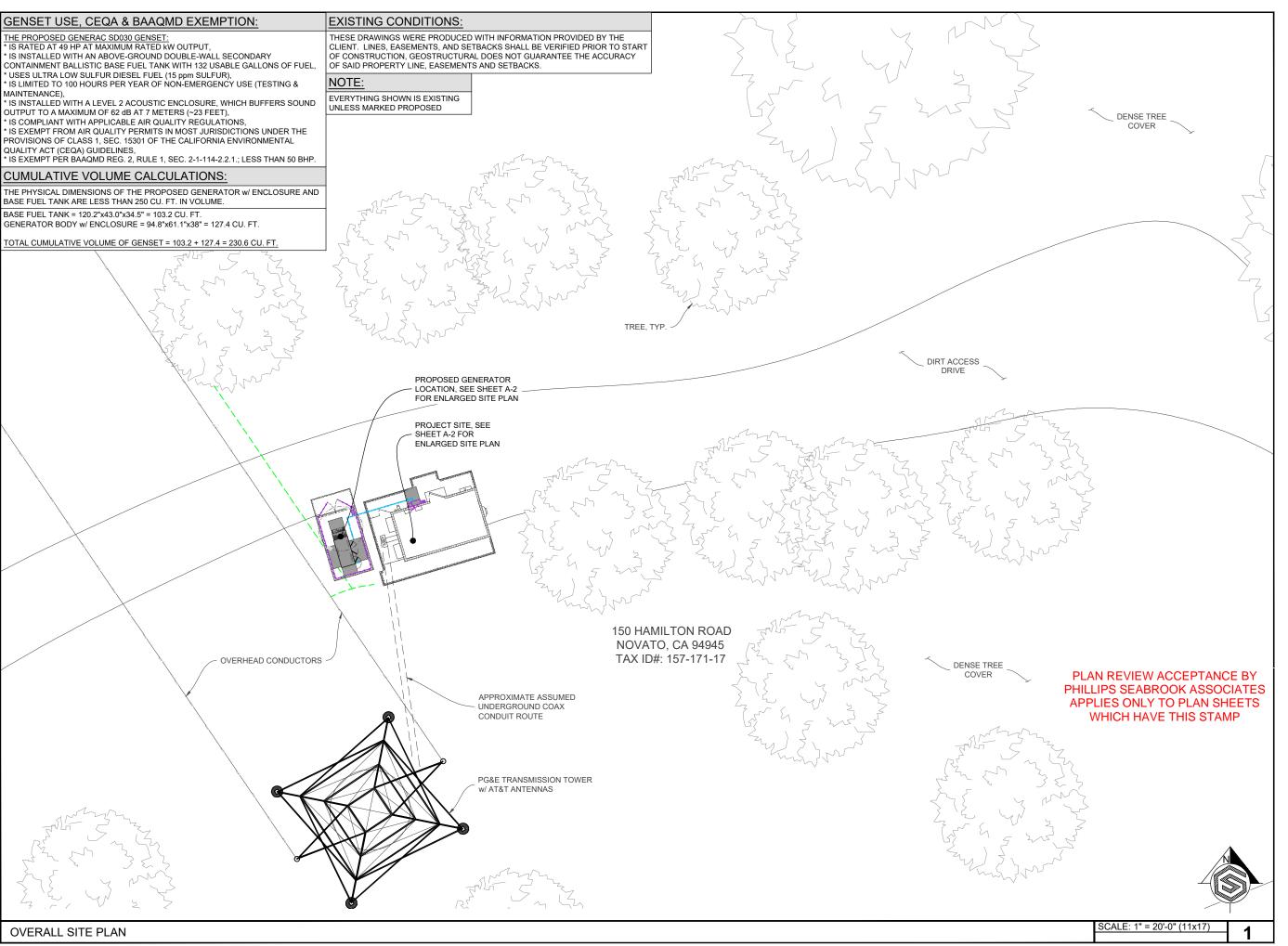
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#### UTILITY NOTE:

THE UTILITIES AS SHOWN ON THIS SET OF DRAWINGS WERE DEVELOPED FROM RECORD INFORMATION. THE INFORMATION PROVIDED IS IMPLIED NOT INTENDED TO BE A COMPLETE INVENTORY OF THE UTILITIES IN THIS AREA. IT IS THE CONTRACTOR'S RESPONSIBILITY TO VERIFY THE LOCATION OF ALL UTILITIES (WHETHER SHOWN OR NOT) AND PROTECT SAID UTILITIES FROM ANY DAMAGE CAUSED BY CONTRACTOR'S ACTIVITIES.

#### **EXISTING CONDITIONS:**

THESE DRAWINGS WERE PRODUCED WITH INFORMATION PROVIDED BY THE CLIENT. LINES, EASEMENTS, AND SETBACKS SHALL BE VERIFIED PRIOR TO START OF CONSTRUCTION, GEOSTRUCTURAL DOES NOT GUARANTEE THE ACCURACY OF SAID PROPERTY LINE, EASEMENTS AND SETBACKS.

#### SCOPE OF WORK DETAILS:

#### GENERAL:

· NEW GENERAC DIESEL GENERATOR PROVIDED BY GENERAL DYNAMICS & INSTALLED BY GENERAL CONTRACTOR. SEE SHEETS E-4.0, E-4.1, E-4.2.

 $\cdot$  NEW CONCRETE PAD PROVIDED & INSTALLED BY GENERAL CONTRACTOR. SEE SHEET S-1.

 $\cdot$  NEW GENERAC AUTOMATIC TRANSFER SWITCH PROVIDED BY GENERAL DYNAMICS & INSTALLED BY CONTRACTOR. SEE SHEETS S-2, E-5.0, E-5.1.

 $\cdot$  NEW COMPOUND FENCE & COMPOUND EXPANSION PROVIDED & INSTALLED BY GENERAL CONTRACTOR. SEE SHEETS S-3, S-4.

· CONTRACTOR TO VERIFY ALL EXISTING UTILITIES PRIOR TO CONSTRUCTION.
· CONTRACTOR SHALL RESTORE & REPAIR ANY DAMAGED AREAS CAUSED BY CONSTRUCTION TO ORIGINAL OR BETTER CONDITION.

 $\cdot$  INNER AND OUTER TANK TESTING DOCUMENTATION SHALL BE PROVIDED ONCE TANK IS IN PLACE ON SITE IN ACCORDANCE WITH NFPA 30.

· A CALIBRATION CHART OF PERMANENT AND DURABLE CONSTRUCTION SHALL BE LOCATED AT THE FILL BOX.

#### CONDUITS:

INSTALL PULL STRING IN EACH CONDUIT.

 $\cdot$  (2) NEW ELECTRICAL CONDUITS WITH CONDUCTORS TO BE INSTALLED FROM NEW GENERATOR TO NEW ATS. CONDUIT PROVIDED AND INSTALLED BY GENERAL CONTRACTOR. SEE SHEETS E-1, E-2.

 $\cdot$  (2) NEW ELECTRICAL CONDUITS WITH CONDUCTORS TO BE INSTALLED FROM NEW GENERATOR TO AC PANEL. CONDUIT PROVIDED & INSTALLED BY GENERAL CONTRACTOR. SEE SHEETS E-1, E-2.

 $\cdot$  (1) NEW ALARM CONDUIT & CABLING PROVIDED & INSTALLED BY GENERAL CONTRACTOR. SEE SHEETS E-1, E-2.

#### GROUNDING:

NEW EXOTHERMIC CONNECTION FROM EXISTING GROUND RING TO NEW MECHANICAL CONNECTION AT GENERATOR CHASSIS. GENERAL CONTRACTOR TO VERIFY LOCATION IN FIELD. LOCATE GROUND RODS NO MORE THAN 8'-0" APART. SEE SHEET E-3.

#### POWER ROUTING KEYED NOTES:

MTS EXISTING AT&T MANUAL TRANSFER SWITCH

INT INTERCEPT EXISTING CONDUIT AND CONDUCTORS AT MTS AND RE-ROUTE THROUGH PROPOSED ATS (~5'). COORDINATE PATH WITH CONSTRUCTION MANAGER

AC EXISTING AC LOAD CENTER

PROPOSED AT&T UNDERGROUND GENERATOR CONDUIT ROUTE (~40').
CONTRACTOR TO LOCATE EXISTING UTILITIES PRIOR TO EXCAVATION.
SEE SHEETS E-1. E-2.

SEE SHEET E-1 FOR SINGLE LINE DIAGRAM.

#### **GENERATOR KEYED NOTES:**

PROPOSED AT&T 30KW DIESEL GENERATOR W/ SOUND ATTENUATED ENCLOSURE, NORMAL/EMERGENCY TANK VENTING AND BASE FUEL TANK. SEE SHEETS S-1, S-2, E-3.

FUEL FILL SHALL BE PROVIDED WITH SPILL CONTROL, WITH A SOLID FILL CONNECTION, AND WITH OVERFILL PREVENTION

FUEL TANK NORMAL AND EMERGENCY VENTS SHALL TERMINATE AT LEAST 12'-0" ABOVE THE ADJACENT GRADE. SEE SHEET S-2.

NFPA 704 PLACARD AND OTHER SIGNAGE. SEE SHEET S-2.

#### ATS / EQUIPMENT KEYED NOTES:

**ENLARGED SITE PLAN** 

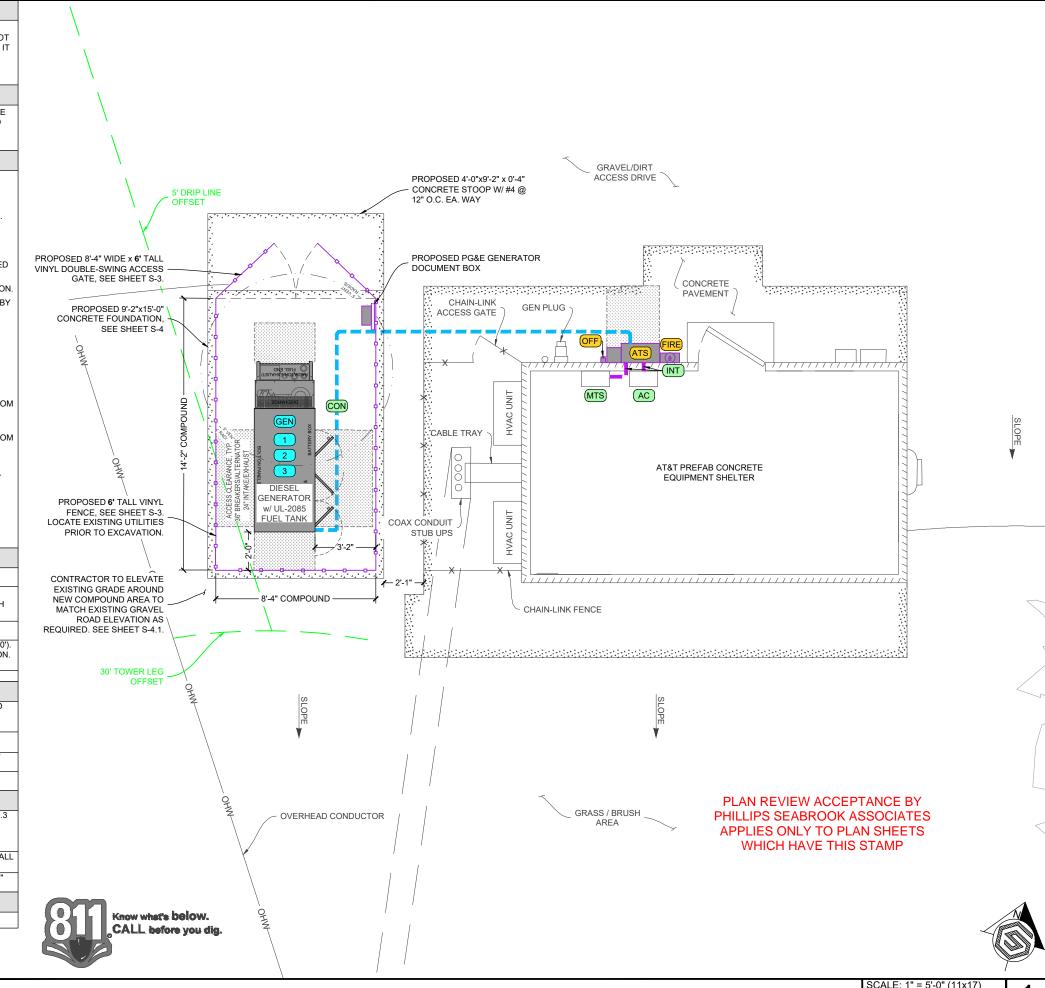
FIRE EXTINGUISHER, (2A-20BC OR APPROVED EQUAL) PER CFC 906.3
-FIRE EXTINGUISHER CABINET (BFC-7009 OR APPROVED EQUAL),
MOUNT TO BUILDING WALL PER CFC 906.9
(5'-0" MAX. ABOVE GRADE)

OFF LOCKABLE EMERGENCY SHUTOFF SWITCH, MOUNT TO BUILDING WALL PER CFC 906.9 (5'-0" MAX. ABOVE GRADE)

PROPOSED ATS w/ CAMLOCK MOUNTED TO BUILDING WALL WITH 36" FRONT CLEARANCE. SEE SHEET S-2.

#### NOTE:

EVERYTHING SHOWN IS EXISTING UNLESS MARKED PROPOSED





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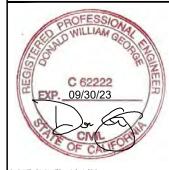
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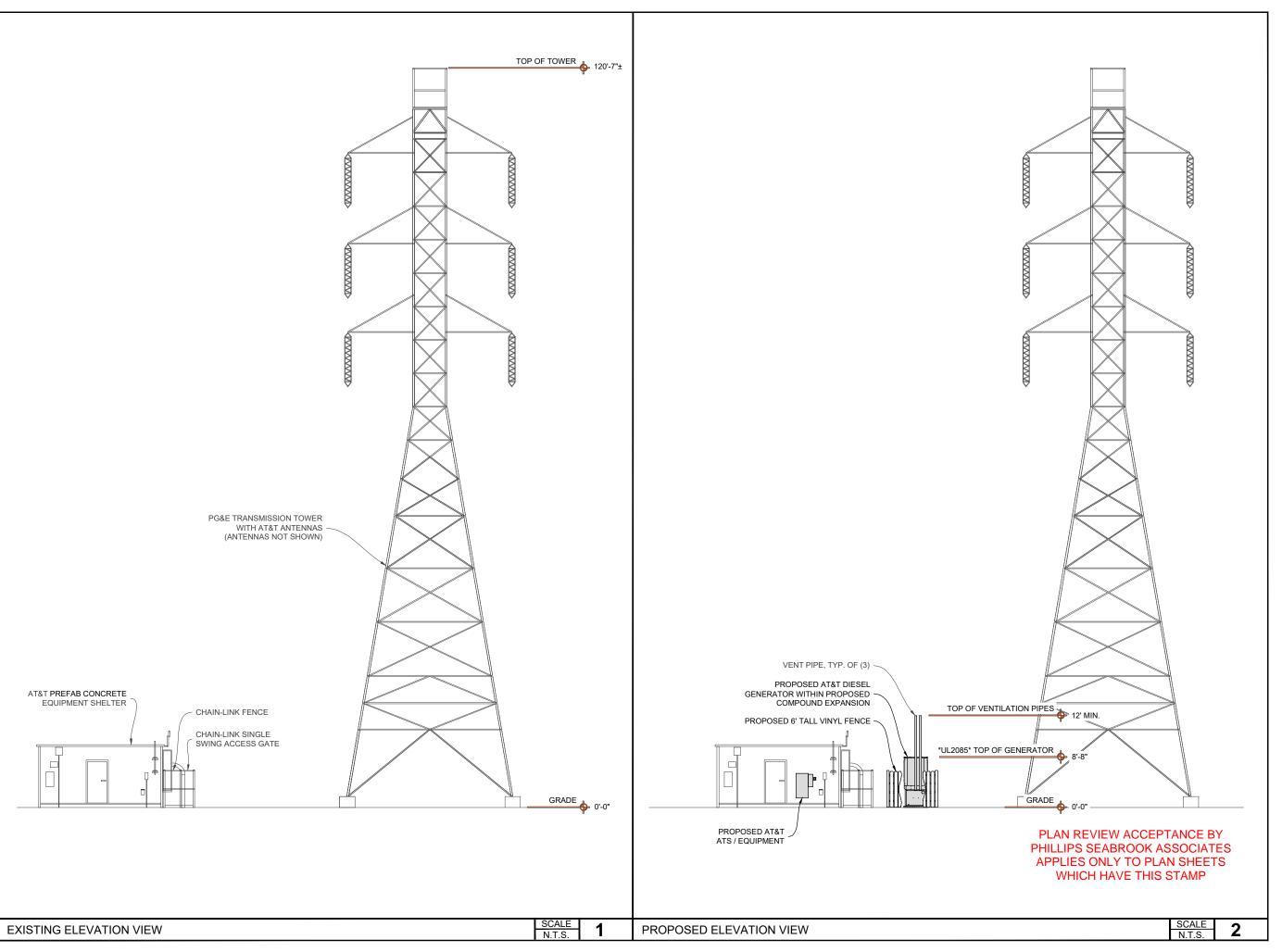
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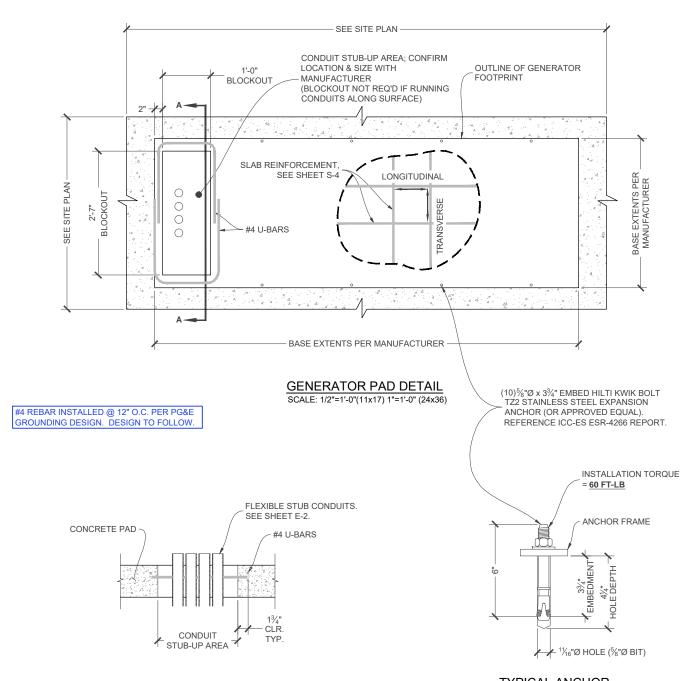
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TYPICAL ANCHOR

**GENERATOR PAD - SECTION A-A** SCALE: 1/2"=1'-0"(11x17) 1"=1'-0" (24x36)

#### STRUCTURAL DESIGN NOTES:

ALL LOADS DERIVED FROM REQUIREMENTS OF THE INTERNATIONAL BUILDING CODE, ASCE 7 & ANSI TIA-222.

BUILDING & COMMUNICATION STRUCTURES: (38.0782481° / -122.5415981°)

WIND LOADS: IBC 2018 & ASCE 7-16

V = 92 MPH ULTIMATE WIND SPEED STRUCTURE CLASS = II; EXPOSURE CATEGORY = C; TOPOGRAPHIC CATEGORY = 1.

IMPORTANCE FACTOR = 1.0.

SEISMIC LOADS: IBC 2018 & ASCE 7-16 STRUCTURE CLASS = II; SITE CLASS = D.

Ss = 1.5; S1 = 0.6; SDS = 1.2

#### CONCRETE NOTES:

- PRIOR TO EXCAVATION. CHECK THE AREA FOR UNDERGROUND FACILITIES
- ALL CONCRETE SHALL BE IN ACCORDANCE WITH CHAPTER 19 OF THE CBC & ACI 318, "BUILDING CODE REQUIREMENTS FOR REINFORCED CONCRETE", LATEST EDITION & HAVE THE FOLLOWING PROPERTIES:
- A MINIMUM 28-DAY COMPRESSIVE STRENGTH (fc) OF 2,500 PSI.
- B CEMENT SHALL BE "LOW-ALKALI" TYPE IIA (MODERATE SULFATE RESISTANCE, AIR ENTRAINING) CONFORMING TO ASTM C150.
- C MAXIMUM WATER/CEMENT RATIO OF 0.45 AND AIR-ENTRAINED 4% TO 7%
- D CONCRETE PROPORTIONING SHALL BE DESIGNED BY AN APPROVED LABORATORY. TOLERANCES IN ACCORDANCE WITH ACI 117. COPIES OF CONCRETE MIX SHALL BE SUBMITTED TO THE ENGINEER FOR REVIEW PRIOR TO PLACEMENT.
- E ALL AGGREGATE USED IN CONCRETE SHALL CONFORM TO ASTM C33. USE ONLY AGGREGATES KNOWN NOT TO CAUSE EXCESSIVE SHRINKAGE. MAXIMUM AGGREGATE SIZE TO BE 3/4"
- F MAXIMUM SLUMP: REFER TO GEOTECHNICAL REPORT WHEN APPLICABLE.
- FORMWORK FOR CONCRETE SHALL CONFORM TO ACI 347. TOLERANCES FOR FINISHED CONCRETE SURFACES SHALL MEET CLASS-C REQUIREMENTS. IN NO CASE SHALL FINISHED CONCRETE SURFACES EXCEED THE FOLLOWING VALUES AS MEASURED FROM NEAT PLAN LINES AND FINISHED GRADES: ± 1/4" VERTICAL, ± 1" HORIZONTAL
- CHAMFER ALL EXPOSED CORNERS AND FILLET ENTRANT ANGLES 3/4" U.N.O.
- CONCRETE FINISHING: CONCRETE SURFACES SHALL BE FINISHED IN ACCORDANCE WITH ACI, PROVIDE ROUGH FINISH FOR ALL SURFACES NOT EXPOSED TO VIEW AND SMOOTH FINISH FOR ALL OTHERS, U.N.O.
- STEEL REINFORCEMENT AND CONCRETE SHOULD BE PLACED IMMEDIATELY UPON COMPLETION OF THE FOUNDATION EXCAVATION. CONTRACTOR SHALL NOT ALLOW A COLD JOINT TO FORM IN THE CONCRETE. PORTION AT GRADE SHOULD BE FORMED. TEMPORARY CASING MAY BE REQUIRED TO PREVENT CAVING PRIOR TO CONCRETE PLACEMENT.

#### REINFORCING STEEL NOTES:

- ALL REINFORCING STEEL SHALL CONFORM TO ASTM A615. VERTICAL/HORIZONTAL BARS SHALL BE GRADE 60: TIES OR STIRRUPS SHALL BE A MINIMUM OF GRADE 40. ALL REINFORCING STEEL SHALL HAVE 3" (± 3/4") OF CONCRETE COVER, U.N.O.
- ALL BAR BENDS, HOOKS, SPLICES AND OTHER REINFORCING STEEL SHALL CONFORM TO THE REQUIREMENTS OF ACI 315.
- ALL BARS SHALL BE SPLICED WITH A MINIMUM LAP OF 48 BAR DIAMETERS. LAP SPLICES OF DEFORMED BARS IN TENSION ZONES SHALL BE CLASS-B SPLICES. WELDING OF BARS IS NOT PERMITTED.
- AT ALL CORNERS AND WALL INTERSECTIONS, PROVIDE BENT HORIZONTAL BARS TO MATCH THE HORIZONTAL REINFORCING STEEL.
- PROVIDE VERTICAL DOWELS IN FOOTINGS AND AT CONSTRUCTION JOINTS TO MATCH VERTICAL REINFORCING BAR SIZE AND SPACING
- ACI-APPROVED PLASTIC-COATED BAR CHAIRS OR PRECAST CONCRETE BLOCKS SHALL BE PROVIDED FOR SUPPORT OF ALL GRADE-CAST REINFORCING STEEL & SHALL BE SUFFICIENT IN NUMBER TO PREVENT SAGGING. METAL CLIPS OR SUPPORTS SHALL NOT BE PLACED IN CONTACT WITH THE FORMS OR THE SUB-GRADE.
- DOWELS AND ANCHOR BOLTS SHALL BE WIRED OR OTHERWISE HELD IN CORRECT POSITION PRIOR TO PLACING CONCRETE. IN NO CASE SHALL DOWELS OR ANCHOR BOLTS BE "STABBED" INTO FRESHLY-POURED CONCRETE.

#### FOUNDATION & SOIL NOTES:

- FOUNDATION DESIGN BASED ON PRESUMPTIVE MINIMUM SOIL PARAMETERS (ALLOWABLE BEARING = 1,000 PSF; ALLOWABLE PASSIVE SLIDING = 100 PSF/FT) IN ACCORDANCE WITH THE IBC AND CBC.
- THE EXCAVATION SHALL BE INSPECTED PRIOR TO THE PLACEMENT OF CONCRETE AND THE CONTRACTOR SHALL PROVIDE A NOTICE OF INSPECTION FOR THE BUILDING INSPECTOR FOR REVIEW AND RECORDS PURPOSES.
- THE CONTRACTOR SHALL DETERMINE THE MEANS AND METHODS NECESSARY TO SUPPORT THE EXCAVATION DURING CONSTRUCTION.
- ALL FOUNDATIONS TO BE PLACED ON FIRM, UNDISTURBED, INORGANIC MATERIAL. PROOF ROLL SUB-GRADE PRIOR TO PLACING CONCRETE WHERE THE MATERIAL HAS BEEN DISTURBED BY EQUIPMENT. UNACCEPTABLE/DISTURBED MATERIAL SHALL BE OVER-EXCAVATED AND REPLACED WITH "LEAN CONCRETE FILL" OR REPLACED WITH STRUCTURAL BACKFILL.
- STRUCTURAL BACKFILL SHALL BE GRANULAR FREE-DRAINING MATERIAL FREE OF DEBRIS, ORGANICS, REFUSE AND OTHERWISE DELETERIOUS MATERIALS. MATERIAL SHALL BE PLACED IN LIFTS NO GREATER THAN 6" IN DEPTH AND COMPACTED TO 95% OF MAXIMUM DENSITY AS DETERMINED PER ASTM D1557 (MODIFIED PROCTOR).

#### MECHANICAL ANCHOR NOTES:

- HILTI PRODUCTS MUST BE INSTALLED IN ACCORDANCE WITH MANUFACTURER'S PRINTED INSTALLATION INSTRUCTIONS, AS INCLUDED IN THE ADHESIVE PACKAGING.
- CONTRACTOR SHALL AVOID DRILLING HOLES IN VERTICAL/HORIZONTAL REINFORCING BARS.
- HOLES MUST BE WIRE BRUSHED AND BLASTED WITH COMPRESSED AIR PRIOR TO INSTALLATION. TEMPERATURES/METHODS/WORKING TIME/ETC. ARE TO BE IN ACCORDANCE WITH MANUFACTURER SPECIFICATIONS.

PLAN REVIEW ACCEPTANCE BY PHILLIPS SEABROOK ASSOCIATES APPLIES ONLY TO PLAN SHEETS WHICH HAVE THIS STAMP



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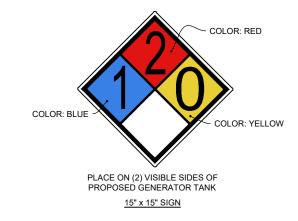
**GENERATOR PAD DETAILS** 

SHEET NUMBER:



PLACE ON (2) VISIBLE SIDES OF PROPOSED GENERATOR TANK

15" x 12" SIGN



FOR FUEL & OTHER **ENVIRONMENTAL EMERGENCIES** CALL EH&S 1-800-566-9347 1-800-KNOW-EHS

PLACE ON (2) VISIBLE SIDES OF PROPOSED GENERATOR TANK 11" x 11" SIGN

AT&T **MOBILITY** 

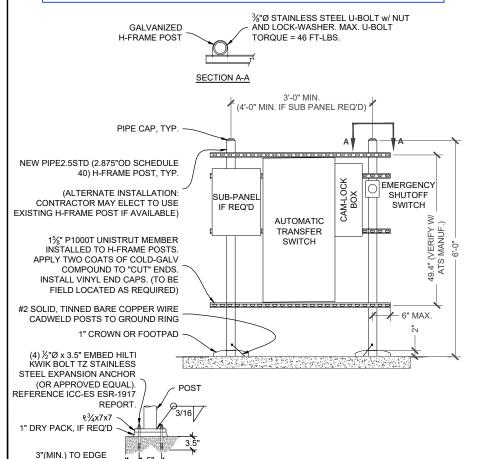
> PLACE ON (2) VISIBLE SIDES OF PROPOSED GENERATOR TANK

> > 6.5" x 3" SIGN

CONTRACTOR TO PROVIDE REQUIRED SIGNAGE FOR ELECTRICAL PANELS, DISCONNECTS, TRANSFER SWITCHES, ETC. PER CALIFORNIA **ELECTRICAL CODE ARTICLE 702.7** 

#### **REQUIRED LABELING & SIGNAGE**

ATS LOCATION SHOWN IN PLANS IS THE BEST AVAILABLE BASED ON THE INFORMATION PROVIDED. ALTERNATIVE LOCATION MAY BE REQUIRED AND SHALL BE APPROVED BY CONSTRUCTION MANAGER AND/OR LANDLORD. THIS DETAIL PROVIDES ALTERNATIVE METHODS OF INSTALLATION (NOT ALL DETAILS MAY BE USED)



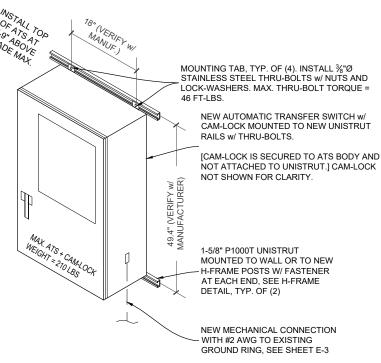
H-FRAME DETAIL (IF REQUIRED)

OF SLAB

FOOT PAD FOR SLAB-TOP INSTALLATION
(IF APPLICABLE)

UNISTRUT WALL	JNISTRUT WALL ATTACHMENT:		
WALL CONSTRUCTION TYPE	FASTENER		
HOLLOW, AT STUD	3/8" DIA. x 2-1/2" EMBED LAG SCREW		
CONCRETE BLOCK (HOLLOW)	3/8" DIA. HILTI HY-270 WITH SCREEN, MINIMUM EMBEDMENT 2-3/8"		
CONCRETE (SOLID)	3/8" DIA. HILTI HY-200, MINIMUM EMBEDMENT 2-3/8"		
NOTES:  1. USE GALVANIZED OR STAINLESS STEEL HARDWARE FOR WALL MOUNT AND CONNECTION OF CHANNELS			

2. GC SHALL USE NON-SHRINKING CAULK TO WEATHER SEAL ALL PENETRATIONS INTO OR THROUGH WALL



ATS MOUNTING DETAIL

#### DIESEL TANK CHECKLIST:

READILY ACCESSIBLE MANUAL SHUTOFF VALVES SHALL BE INSTALLED ON SUPPLY PIPING AT THE POINT O USE AND THE TANK (CFC 5003.2.2.1)

SECONDARY CONTAINMENT-TYPE TANKS SHALL BE UL LISTED, UL-2085, AND COMPLY WITH ALL OF THE FOLLOWING REQUIREMENTS; OTHERWISE TRADITIONAL SPILL CONTROL OR SECONDARY CONTAINMENT MEASURES, SUCH AS DIKING, SHALL BE UTILIZED (NFPA 30 22.11.4)

- CAPACITY OF DIESEL TANK SHALL NOT EXCEED 50,000 GAL
- PIPING CONNECTIONS SHALL BE ABOVE THE LIQUID LEVEL
- MEANS SHALL BE PROVIDED TO PROTECT RELEASE OF LIQUID BY SIPHON FLOW.
- MEANS TO DETERMINE LIQUID LEVEL IN TANK SHALL BE PROVIDED TO DRIVER.
- MEANS TO PREVENT OVERFILLING BY AN ALARM AT 90% CAPACITY AND AUTOMATICALLY STOPPING DELIVERY OF LIQUID TO THE TANK AT 95% CAPACITY.
  - SPACING BETWEEN ADJACENT TANKS SHALL NOT BE LESS THAN 3'
- TANK SHALL BE PROTECTED AGAINST DAMAGE FROM VEHICLES.
- INTERSTITIAL SPACE SHALL HAVE EMERGENCY VENTING.
- INTEGRITY OF SECONDARY CONTAINMENT SHALL BE ESTABLISHED.
- THE SECONDARY CONTAINMENT SHALL WITHSTAND THE HYDROSTATIC HEAD OF THE MAXIMUM AMOUNT OF LIQUID STORED IN THE PRIMARY TANK.

# TANK LABELING AND PROTECTIONS:

THE FOLLOWING SIGNS AND LABELS SHALL BE AFFIXED TO THE TANK

- "DIESEL FUEL NO SMOKING" (CFC 5703.5 & CFC 5003.7.1)
- NFPA 704 PLACARD (CFC 5003.5)
- EH&S
- + AT&T MOBILITY SIGN #3

CRASH PROTECTION COMPLYING WITH FC 312 SHALL BE PROVIDED (CFC 5003.9.3) (IF APPLICABLE)

#### **GENERATOR FEATURES:**

GENERATORS SHALL BE UL 2200 LISTED AND COMPLY WITH NFPA 37 AND NFPA 110. (CFC 604.1 AND 604.1.1) INSTALLATIONS SHALL HAVE A LABELED REMOTE MANUAL STOP (NFPA 110 5.6.5.6 & 5.6.5.6.1 AND NFPA 37

#### DOUBLE WALL FUEL TANK BASE SPECIFICATION:

REF: AT&T 30KW GENERATOR PACKAGE

UL REGISTRATION NUMBER: MH 1848

UL-2085 DOUBLE WALL FUEL TANK BASE SPECIFICATION

FUEL TANK BASE CONSTRUCTION:

- BE CONSTRUCTED IN ACCORDANCE WITH UNDERWRITERS LABORATORIES STANDARD UL-2085. BE CONSTRUCTED IN ACCORDANCE WITH FLAMMABLE COMBUSTIBLE LIQUIDS CODE, NFPA 30; THE STANDARD FOR INSTALLATION USE OF STATIONARY COMBUSTIBLE ENGINE GAS TURBINES, NFPA 37; AND THE STANDARD FOR EMERGENCY STANDBY POWER SYSTEMS, NFPA 110.
- MINIMUM ANCHOR QUANTITY PER MANUFACTURER OR THIS PLAN SET; WHICHEVER IS LARGER.

SUB BASE TANK TESTING

- PRIMARY TANK & SECONDARY CONTAINMENT BASIN SECTIONS SHALL BE PRESSURIZED AT 3-5 PSI AND LEAK-CHECKED TO ENSURE INTEGRITY OF SUB BASE WELD SEAMS PER UL-142 STANDARDS FUEL FILL: 2.5 - 5 GALLON SPILL CONTAINMENT WITH ALARM
- 40% REMAINING FOR ALARM
- 20% REMAINING FOR SHUT-DOWN

FACTORY PRE-SET AT 90% FULL FOR ALARM

SUB BASE TANK SHALL INCLUDE A WELDED STEEL CONTAINMENT BASIN, SIZED AT A MINIMUM OF 110% OF THE TANK. CAPACITY TO PREVENT ESCAPE OF FUEL INTO THE ENVIRONMENT IN THE EVENT OF A TANK RUPTURE. A FUEL CONTAINMENT BASIN LEAK DETECTOR SWITCH SHALL BE PROVIDED.

#### **NEPA NOTES:**

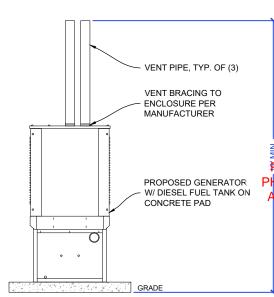
- CONSTRUCTION, INSTALLATION MAINTENANCE, & OPERATIONAL TESTING OF EPSS SHALL COMPLY WITH THE LATEST ADOPTED **EDITION OF NFPA 110**
- ALL ELECTRICAL WORK SHALL COMPLY WITH LATEST ADOPTED EDITION OF NFPA 70 - NATIONAL **ELECTRICAL CODE**

# FUEL TANK NOTES:

THE TANK SHALL BE MANUFACTURED WITH THE FOLLOWING: -INTERSTITIAL ELECTRONICALLY MONITORED RUPTURE BASIN -ALARM TO MONITOR THE SPACE BETWEEN THE PRIMARY AND SECONDARY TANK -OVERFILL ALERT TO VISUALLY WARN WHEN THE TANK IS FILLED UPON CAPACITY -OVERSPILL CONTAINMENT AT FILL PORT TO PREVENT SPILL OF FUEL

DURING FILLING OPERATIONS. -2.5/5 GALLON OVERSPILL CONTAINMENT W/ LOCKABLE CAP.

> \*SEE SHEETS E-4.3, E-4.4 FOR VENT PIPES FUEL FILL SPILL & ALARM COMPONENTS



GENERATOR VENTING DETAIL



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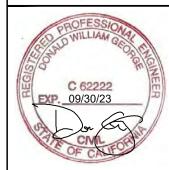
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	REVISIONS		
REV	DATE	DESCRIPTION	
2	06/14/22	PGE GG	JAD
1 02/15/22		PGE REDLINES	
0	01/05/22	ISSUED FOR CONSTRUCTION	KS

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SITE INFORMATION:

HWY 101 - IGNACIO

10088152

GENERATOR INSTALLATION **PROJECT** 

> 150 HAMILTON ROAD NOVATO, CA 94945

JURISDICTION USE

**REVIEW ACCEPTANCE BY** PS SEABROOK ASSOCIATES ES ONLY TO PLAN SHEETS WHICH HAVE THIS STAMP

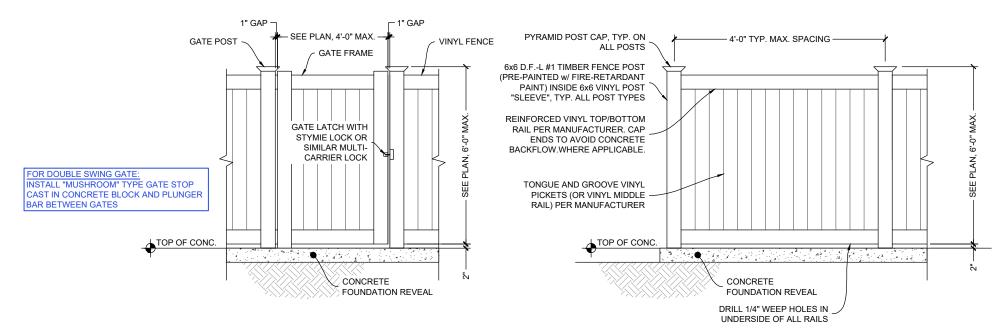
SHEET TITLE:

**GENERAL** STRUCTURAL DETAILS

SHEET NUMBER:

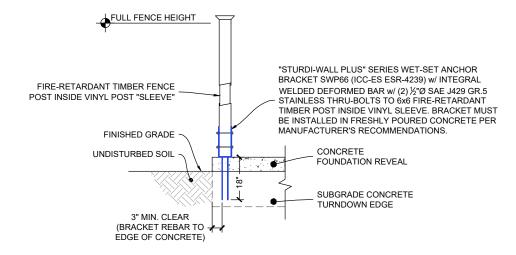
#### VINYL FENCE NOTES:

- 1. CONTRACTOR TO REFER TO FENCE MANUFACTURER'S INSTALLATION GUIDELINES.
- ALL VINYL FENCE PRODUCTS SHALL BE "COMMERCIAL" OR "PROFESSIONAL" GRADE WITH UV INHIBITORS AND IMPACT MODIFIERS.
- 3. FENCES INSTALLED ON SLOPED GRADES SHALL BE STEPPED OR RACKED AS ALLOWED BY MANUFACTURER.
- 4. All VINYL FENCE PRODUCTS TO BE FIRE-RESISTANT AND NON CONDUCTIVE. USE "FIBERFENCE" OR APPROVED EQUIVALENT PER PG&E REQUIREMENTS.
- TIMBER FENCE POSTS SHALL BE TREATED D.F.-L #1 OR BTR. POSTS TO BE PAINTED WITH FIRE-RETARDANT PAINT PER PG&E REQUIREMENTS PRIOR TO "SLEEVING" WITH "FIBERFENCE" VINYL POST MATERIAL.



### VINYL ACCESS GATE DETAIL

VINYL PRIVACY FENCE DETAIL



BRACKET AT POST DETAIL

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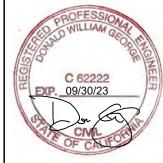


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REVISIONS			
		INT	
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ATE SIGNED: 6/14/22

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GENERATOR INSTALLATION PROJECT

150 HAMILTON ROAD NOVATO, CA 94945

JURISDICTION USE:

SHEET TITLE:

FENCE & GATE DETAILS

SHEET NUMBER:

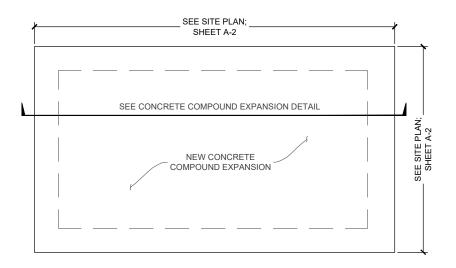
S4.2
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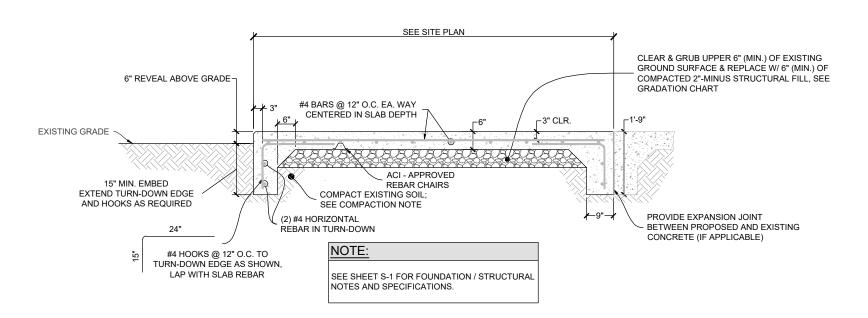
<u>AG</u>	AGGREGATE NOTES:				
1	THE AGGREGATE MATERIAL TO BE USED WILL BE PRODUCED FROM SOUND, TOUGH, DURABLE ROCK AND SHALL BE UNIFORM IN QUALITY AND GRADATION. THE CRUSHED MATERIAL WILL BE REASONABLY FREE FROM SOFT OR DISINTEGRATED PIECES, ORGANIC MATERIALS, AND OTHER OBJECTIONABLE MATTER.				
2	THE AGGREGATE MATERIAL WILL SHOW A LOSS LESS THAN 35% IN THE LOS ANGELES ABRASION TEST.				
3	THE PERCENTAGE OF SOFT PARTICLES, AS DETERMINED BY THE CLAY LUMPS AND FRIABLE PARTICLES [AASHTO T 112], SHALL NOT BE MORE THAN 5%.				
4	THE AGGREGATE MATERIAL USED WILL NOT HAVE A SAND EQUIVALENT LESS THAN 30 IF 5% OR MORE OF THE MATERIAL PASSES THE NUMBER 200 SIEVE.				
5	80% OF THE GRAVEL (BY WEIGHT) OF THE COMBINED COURSE AGGREGATE SHALL HAVE THREE OR MORE ROUGH ANGULAR SURFACES AND PRODUCED BY CRUSHING OF THE ROCK.				
6	THE PLASTICITY INDEX OF THE FINISHED AGGREGATE PRODUCT SHALL NOT EXCEED 6.				

AGGREGATE GRADATION CHART:				
	(% BY WEIGHT PASSING SIEVES)			
SIEVE SIZE 2"-MINUS ¾"-MINUS				
2½"	100	-		
2"	-			
1" 55-83		100		
3/4" -		90-100		
No. 4	No. 4 30-60			
No. 8	30-50			
No. 30	-			
No. 200 0-8 3-9				

#### COMPACTION NOTE:

STRUCTURAL FILL SHALL BE GRANULAR FREE-DRAINING MATERIAL FREE OF DEBRIS, ORGANICS, REFUSE AND OTHERWISE DELETERIOUS MATERIALS. MATERIAL SHALL BE PLACED IN LIFTS NO GREATER THAN 12" IN DEPTH AND COMPACTED TO 95% OF MAXIMUM DENSITY AS DETERMINED PER ASTM D1557.





PLAN REVIEW ACCEPTANCE BY
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CONCRETE COMPOUND EXPANSION DETAIL



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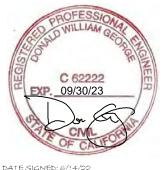
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	REVISIONS				
REV	DATE	DESCRIPTION	INT		
2	06/14/22	PGE GG	JAD		
1	02/15/22	PGE REDLINES	JAD		
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GENERATOR INSTALLATION PROJECT

150 HAMILTON ROAD NOVATO, CA 94945

JURISDICTION USE:

SHEET TITLE:

COMPOUND EXPANSION DETAIL

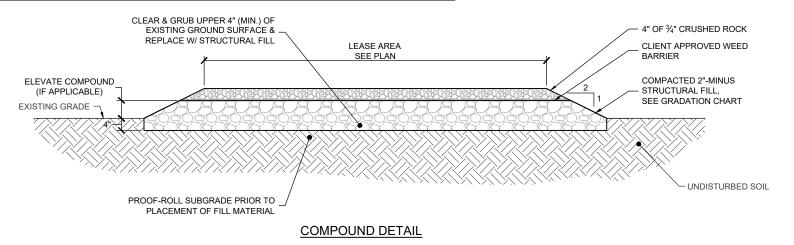
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No. 30 10-25		-		
No. 200	3-9			

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2	06/14/22	PGE GG JAE			
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ATE SIGNED: 6/14/22

SITE INFORMATION:

HWY 101 - IGNACIO

10088152

GENERATOR INSTALLATION PROJECT

150 HAMILTON ROAD NOVATO, CA 94945

JURISDICTION USE:

SHEET TITLE:

GRADE BUILD-UP DETAIL

SHEET NUMBER:

S-4.1

	NDUIT / WIRE S	CHEDULE:				
NO.	FROM	ТО	WIRES	GROUND	CONDUIT SIZE	FUNCTION
1	NORMAL POWER SOURCE	AUTOMATIC TRANSFER SWITCH	(3) W/C	(1) W/C	(1) W/C	NORMAL POWER FEEDER TO ATS (CUT BACK EXISTING)
2	AUTOMATIC TRANSFER SWITCH	LOAD CENTER	(3) W/C	(1) W/C	(1) W/C	POWER FEEDER FROM ATS TO PANELS
3	GENERATOR	AUTOMATIC TRANSFER SWITCH	(3) W/C	(1) W/C	(1) W/C	STANDBY POWER FEEDER TO ATS
4	AUTOMATIC TRANSFER SWITCH	GENERATOR	(2) W/C	(1) W/C	(1) W/C	START CIRCUIT
(5)	LOAD CENTER (DISTRIBUTION CENTER)	GENERATOR, ATS	(2) W/C (2) W/C (2) W/C	(1) W/C (1) W/C (1) W/C	(1) W/C (1) W/C (1) W/C	CKT FOR GEN BLOCK HEATER & BATTERY HEATER, CKT FOR BATTERY CHARGER, CKT FOR ATS CONTROLS (SEE BREAKER NOTE)
6	GENERATOR	THROUGH ATS TO ALARM BLOCK	12-PAIR 24 AWG OR 2EA 6-PAIR CAT5	N/A	1"	ALARM CABLES (1) 12 PAIR 24 AWG. PROVIDE 24" OF SLACK CABLE. FINAL PUNCH DOWN IS BY AT&T TECH. LABEL ALL WIRES
7	AUTOMATIC TRANSFER SWITCH	ALARM BLOCK	(2) 12-PAIR 24 AWG OR (2) 6-PAIR CAT5 (1) 1-PAIR 24AWG	N/A	1"	ALARM CABLES (1) 12 PAIR 24 AWG (RUN THRU INTERIOR OF SHELTER OR GROUND EQUIPMENT & INTO ALARM BOX). PROVIDE SINGLE PAIR FOR COMMERCIAL POWER FAIL ALARM. PROVIDE 24" OF SLACK CABLE. FINAL PUNCH DOWN IS BY AT&T TECH. LABEL ALL WIRES
8	CAM-LOCK BOX	AUTOMATIC TRANSFER SWITCH	(3) W/C	(1) W/C	(1) W/C	STANDBY POWER FEEDER TO ATS
		(1	N/C) = SEE WIRE/	CONDUIT	SIZING TAB	LE FOR VALUES
ATS	POLE NOTE:					
PHAS ATS T UNU	E OPERATION. IN SIN TO BE INSTALLED WIT	ONFIGURABLE FOR SII GLE PHASE INSTALLAT H ONE POLE NOT CON FIGURED FOR DUAL-PO WITCHED	TIONS, 3-POLE NECTED			EXISTING 120/240, 1PH, 200 PANEL AT EQUII  (2) OR (3) NEW 20A WITH ADEQUATE KAIC RATING

	ALARM WIRE IDENTIFICATION CHART:			
1	WIRE	ALARM		
	BROWN BROWN / WHITE	GENERATOR RUNNING		
	GREEN GREEN / WHITE	CRITICAL FAULT		
	BLUE BLUE / WHITE	MINOR FAULT		
	ORANGE ORANGE / WHITE	LOW FUEL		
1	BROWN * BROWN / WHITE *	FUEL LEAK		
ĺ	*CAT5 CABLE ONL	Y. FROM 2ND CAT5 CABLE		

FEED/DISTRIBUTION PANEL \*CONTRACTOR TO UTILIZE NEXT AVAILABLE IN SEQUENCE SINGLE BREAKER POSITION FOR

GENERATOR, BATTERY CHARGER, BATTERY HEATER AND BLOCK HEATER

CONTRACTOR TO VERIFY VOLTAGE AND PHASE OF PROPOSED ATS/CAMLOCK AND GENERATOR ARE COMPATIBLE W/ EXISTING SERVICE

**EXISTING DISTRIBUTION PANEL** 

EXISTING PANEL SCHEDULE INFORMATION WAS NOT AVAILABLE AT THE TIME OF DRAWING CREATION.

SCOPE OF WORK REQUIRES (2) OR (3) PROPOSED SINGLE POLE, 20A BREAKERS, ONE EACH FOR CONDUIT CALLOUT NUMBER 5 ON THE SINGLE LINE DIAGRAM. UTILIZE EMPTY OR SPARE SPACES ON EXISTING PANELBOARD IF POSSIBLE.

IF SUFFICIENT SPACES ARE NOT PRESENT IN MAIN PANEL, PROVIDE NEW SUBPANEL FED WITH NEW SINGLE-POLE, 60A BREAKER IN MAIN PANELBOARD. SQUARE D QO LOAD CENTER RECOMMENDED AS NECESSARY.

> ALL ELECTRICAL WORK CONDUCTED ON PANELS TO BE VERIFIED WITH CONSTRUCTION MANAGER AND CONDUCTED BY AN APPROVED ELECTRICAL CONTRACTOR LICENSED IN THE STATE

#### PANEL NOTES:

- CONTRACTOR TO LABEL WIRES WITH P-TOUCH OR SIMILAR LABELS ONLY. ABSOLUTELY NO HANDWRITTEN
- CONTRACTOR SHALL PERFORM A POWER STUDY ON EXISTING AC PANEL PRIOR TO INSTALLING, CHANGING, ALTERING, OR REMOVING ANY BREAKER. NO WORK SHALL BE COMPLETED ON AC PANEL WITHOUT PROPER INSPECTOR OR ENGINEER APPROVED DOCUMENTATION CONFIRMING CAPACITY ON SITE. ALL WORK SHALL CONFORM TO CEC VERSION ENFORCED BY A.H.J. AT TIME OF INSTALLATION.
- CONTRACTOR SHALL VERIFY THAT THE MAXIMUM DEMAND FOR ALL CONNECTED EQUIPMENT AT THIS SITE AS CALCULATED PER CEC DOES NOT EXCEED THE GENERATOR OUTPUT CIRCUIT BREAKER RATING. (SEE NOTE #4
- IF MAXIMUM DEMAND OF GENERATOR OUTPUT CIRCUIT BREAKER RATING AS CALCULATED PER CEC IS CONTINGENT ON THE TWO HVAC UNITS NOT OPERATING CONCURRENTLY, THEN CONTRACTOR SHALL VERIFY THAT THE HVAC LEAD/LAG CONTROLLER IS CONFIGURED TO PREVENT CONCURRENT OPERATION. IF NOT. THEN CONTRACTOR SHALL RECONFIGURE IT AS NEEDED TO PREVENT TRIPPING THE CIRCUIT BREAKER.
- SEE REQUIRED LABELING & SIGNAGE: SHEET S-2

#### PLAN REVIEW ACCEPTANCE BY | WIRE/CONDUIT SIZING: FEEDER MAX 1-WAY LENGTH IN FEET PHILLIPS SEABROOK ASSOCIATES WIRE SIZE APPLIES ONLY TO PLAN SHEETS WHICH HAVE THIS STAMP 1/0 2/0 3/0 4/0 250 KCMIL 300 KCMIL GENERATOR NEUTRAL SHALL NOT BE BONDED 350 KCMIL BE SOLIDLY CONNECTED THROUGH THE ATS, 400 KCMII WITH NO SWITCHING DEVICE INSERTED IN THE 500 KCMII 600 KCMII NEUTRAL AT GENERATOR) THIS GENERATOR 750 KCMIL

150A OCP 150A OCP 200A OCP 200A OCP 200A OCP GROUND CONDUIT 150A OCP 120/208V 1P 208Y/120V 3P 120/240V 1P 208Y/120V 3P WIRE SIZE SIZE 120/240V 1P 120/208V 1P 1-1/2" 192 227 196 227 #4 2" 213 213 284 284 185 #4 2" #4 2" 337 337 253 220 254 #4 2-1/2" 378 284 423 423 318 275 318 #3 2-1/2" 471 471 354 307 354 #2 2-1/2" 510 510 383 332 383 #2 3" 503 581 436 378 436 #1 3" 625 625 469 469 1/0 3-1/2" 601 521 521 2/0 3-1/2" 3/0

FEEDER MAXIMUM LENGTH VALUES SHOWN ARE FOR MAX. FEEDER VOLTAGE DROP OF 2.5%. NOTE THAT A 30KW GENERATOR REQUIRES NO MORE THAN 150A OCP.

	INCREASED GROU	JND WIRE SIZE - BELOW G	ROUND
WIRE SIZE	DISTANCE	GROUND WIRE SIZE	CONDUIT SIZE
#12	0 - 51 FT	#12	1"
#10	52 - 85 FT	#10	1"
#8	86 - 130 FT	#8	1"
#6	131 - 203 FT	#6	1"

MAX. ONE-WAY LENGTH VS. WIRE SIZE FOR 20A CKT, AND CEC REQ'D

FOR LONG RUNS, PER CEC 300.3(B)(1), FOR CONDUCTORS 1/O AND LARGER. CONTRACTOR MAY ELECT TO INSTALL FOUIVALENT SETS OF PARALLEL CONDUCTORS (UPSIZE GROUND WIRE AND CONDUIT ACCORDINGLY). SMALLER CONDUCTORS REQUIRING UPSIZING MUST BE REPLACED w/ ADEQUATELY SIZED LARGER CONDUCTORS



**GENERAL DYNAMICS** Information Technology



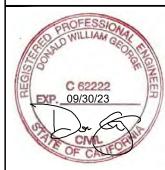
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GENERATOR INSTALLATION **PROJECT** 

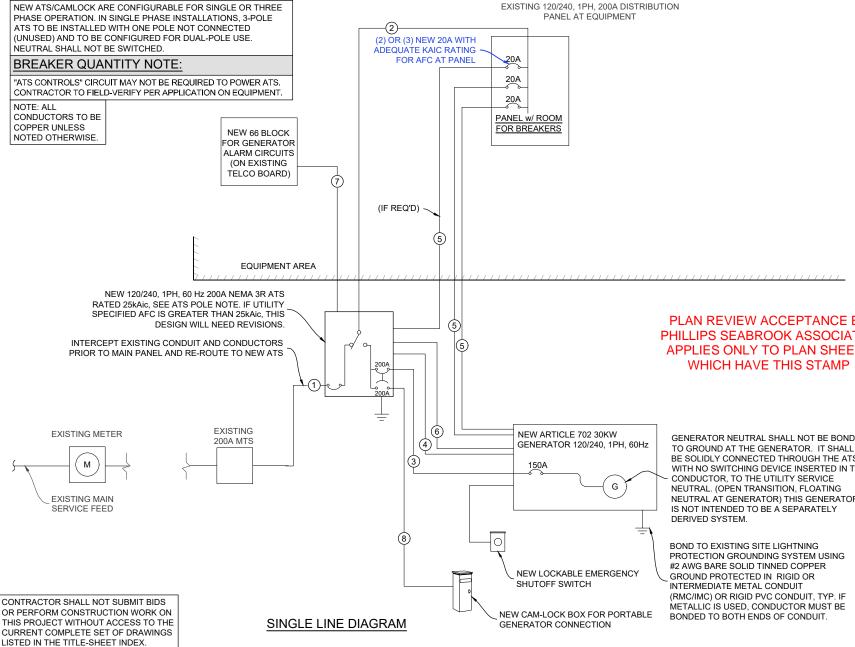
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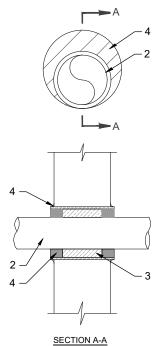
JURISDICTION USE

SHEET TITLE:

**ELECTRICAL DETAILS** 

SHEET NUMBER:





IF EXISTING CONSTRUCTION VARIES FROM THIS DETAIL, AN EQUAL 3-HR U.L. PENETRATION APPROPRIATE FOR THE EXISTING WALL TYPE SHALL BE CONSTRUCTED

GC SHALL USE NON-SHRINKING CAULK TO WEATHERSEAL ALL PENETRATIONS INTO OR THRU SHELTER WALL.

# U.L. SYSTEM NO. C-AJ-1150 CONDUIT THROUGH BEARING WALL SIMILAR TO U.L. DESIGN NO. U902 F RATING = 3 HR

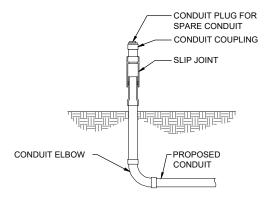
- FLOOR OR WALL ASSEMBLY: MINIMUM 4-1/2" THICK REINFORCED LIGHTWEIGHT OR NORMAL WEIGHT (100-150 PCF) CONCRETE. WALL MAY ALSO BE CONSTRUCTED OF ANY UL CLASSIFIED CONCRETÉ BLOCKS\*. MAX DIAMETER OF OPENING IS 4". (SEE CONCRETE BLOCKS 9CATZ) CATEGORY IN THE FIRE RESISTANCE DIRECTORY FOR NAMES OF MANUFACTURERS.
- 2. THROUGH PENETRATIONS: ONE METALLIC PIPE OR CONDUIT TO BE RIGIDLY SUPPORTED ON BOTH SIDES OF FLOOR OR WALL ASSEMBLY. THE ANNULAR SPACE SHALL BE MINIMUM 0". (POINT CONTACT) TO MAXIMUM 1-3/8". THE FOLLOWING TYPES AND SIZES OF METALLIC PIPES OR CONDUITS MAY BE USED:
  - A. STEEL PIPE-NOMINAL 6" DIAMETER (OR SMALLER) SCHEDULE 40 (OR HEAVIER) STEEL PIPE B. IRON PIPE-NOMINAL 6" DIAMETER (OR SMALLER) CAST OR DUCTILE IRON PIPE.
    C. CONDUIT - NOMINAL 4" DIAMETER (OR SMALLER) STEEL ELECTRICAL METALLIC TUBING OR NOMINAL 3-1/2" DIAMETER (OR SMALLER) STEEL CONDUIT.
- 3. PACKING MATERIAL: MINIMUM 6" THICKNESS OF MIN 4.0 PCF MINERAL WOOL BATTING INSULATION FIRMLY PACKED INTO OPENING AS A PERMANENT FORM. PACKING MATERIAL TO BE RECESSED FROM TOP SURFACE OF FLOOR OR FROM BOTH SURFACES OF WALL AS REQUIRED TO ACCOMMODATE THE REQUIRED THICKNESS OF FILL
- 4. FILL, VOID, OR CAVITY MATERIAL\*: SEALANT: MINIMUM 1/4" THICKNESS OF FILL MATERIAL APPLIED WITHIN THE ANNULUS, FLUSH WITH TOP SURFACE OF FLOOR AND WITH BOTH SURFACES OF WALL. AT THE POINT CONTACT LOCATION BETWEEN PIPE AND CONCRETE, A MINIMUM 1/2" DIAMETER BEAD OF FILL MATERIAL SHALL BE APPLIED AT THE CONCRETE/PIPE INTERFACE ON THE TOP SURFACE OF FLOOR AND ON BOTH SURFACES OF WALL. W-RATING APPLIES ONLY WHEN CP601S OR CP604 SEALANT IS

HILTI CONSTRUCTION CHEMICALS, DIV OF HILTI INC. : CP601S, CP604, CP606, OR FS-ONE SEALANT.

\* BEARING THE UL CLASSIFICATION MARK

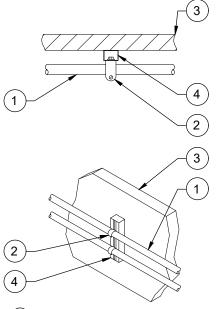
#### **CONDUIT NOTES:**

- VERIFY WIRE AND CONDUIT QUANTITY & SIZES WITH GENERATOR MAKE & MODEL # PRIOR TO INSTALLATION. VERIFY ELECTRICAL REQUIREMENTS WITH
- ALL CONDUIT ABOVE GRADE OR IN AREAS OF HIGH TRAFFIC SHALL BE SCH 80
- PROVIDE SCH 40 PVC CONDUIT BELOW GRADE EXCEPT AS NOTED BELOW.
- PROVIDE RGS CONDUIT AND ELBOWS AT STUB UP LOCATIONS (I.E. SERVICE POLE, BTS EQUIPMENT, ETC.)
- INSTALL UTILITY PULLBOXES PER CEC.



#### SLIP JOINT DETAIL (IF APPLICABLE)

# OUTER WALL PENETRATION DETAIL (IF APPLICABLE)



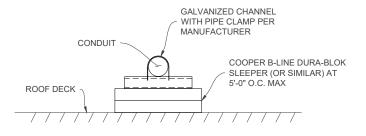
- (1) CONDUIT (TYP)
- (2) P1119 OR P2558 CLAMP
- (3) EXISTING WALL/CEILING
- VERTICAL "UNISTRUT" P1000T (4) REQUIRED LENGTH BASED ON QUANTITY OF CONDUIT TO BE MOUNTED. INSTALL AT 5'-0" O.C. MAX. W/ FASTENER AT EACH END.

CONDUIT WALL MOUNT DETAIL (IF APPLICABLE)

UNISTRUT WALL ATTACHMENT: WALL CONSTRUCTION FASTENER HOLLOW, AT STUD 3/8" DIA. x 2-1/2" EMBED LAG SCREW CONCRETE BLOCK 3/8" DIA. HILTI HY-270 WITH SCREEN, (HOLLOW) MINIMUM EMBEDMENT 2-3/8" 3/8" DIA. HILTI HY-200. (SOLID) MINIMUM EMBEDMENT 2-3/8"

1. USE GALVANIZED OR STAINLESS STEEL HARDWARE FOR WALL MOUNT AND CONNECTION OF CHANNELS

2. GC SHALL USE NON-SHRINKING CAULK TO WEATHER SEAL ALL PENETRATIONS INTO OR THROUGH WALL



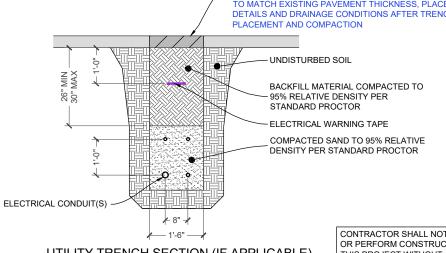
ROOF CONDUIT MOUNTING DETAIL (IF APPLICABLE)

#### **CONDUIT NOTES:**

- VERIFY WIRE AND CONDUIT QUANTITY & SIZES WITH GENERATOR MAKE & MODEL # PRIOR TO INSTALLATION. VERIFY ELECTRICAL REQUIREMENTS WITH LOCAL UTILITY PROVIDER.
- ALL CONDUIT ABOVE GRADE OR IN AREAS OF HIGH TRAFFIC SHALL BE SCH 80
- PROVIDE SCH 40 PVC CONDUIT BELOW GRADE EXCEPT AS NOTED BELOW.
- PROVIDE RGS CONDUIT AND ELBOWS AT STUB UP LOCATIONS (I.E. SERVICE POLE, BTS EQUIPMENT, ETC.)
- INSTALL UTILITY PULLBOXES PER CEC.

CONTRACTOR TO MATCH EXISTING GRADE CONDITIONS AFTER TRENCH PLACEMENT AND COMPACTION

(FOR PAVEMENT) CONTRACTOR TO SAW-CUT AND REMOVE EXISTING PAVEMENT. UPON REPLACEMENT, CONTRACTOR TO MATCH EXISTING PAVEMENT THICKNESS, PLACEMENT DETAILS AND DRAINAGE CONDITIONS AFTER TRENCH



UTILITY TRENCH SECTION (IF APPLICABLE)

CONTRACTOR SHALL NOT SUBMIT BIDS OR PERFORM CONSTRUCTION WORK ON THIS PROJECT WITHOUT ACCESS TO THE CURRENT COMPLETE SET OF DRAWINGS LISTED IN THE TITLE-SHEET INDEX



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SITE INFORMATION:

HWY 101 - IGNACIO

10088152

GENERATOR INSTALLATION **PROJECT** 

> 150 HAMILTON ROAD NOVATO, CA 94945

JURISDICTION USE:

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SHEET TITLE:

**ELECTRICAL DETAILS** 

SHEET NUMBER:

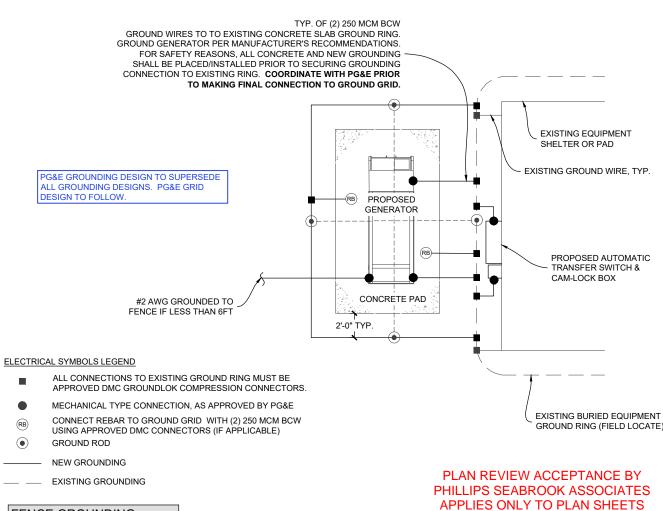
E-2

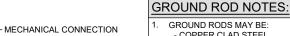
#### PG&E NOTES:

- IF THIS GROUNDING DIAGRAM CONFLICTS WITH PG&E REQUIREMENTS, PG&E GROUNDING PLAN WILL
- CONTRACTOR TO EXERCISE CAUTION AROUND EXISTING GROUND SYSTEM. ANY DAMAGE DONE TO PG&E CONDUCTORS/GROUND COMPONENTS MUST BE REPAIRED/REPLACED TO THE SATISFACTION OF PG&E AT THE EXPENSE OF THE CONTRACTOR.

#### **GROUNDING NOTES:**

- IF MORE THAN 20' FROM EXISTING GROUND RING, INSTALL GROUND ROD (5/8" x 10' SS). ROD SPACING: 8' MAX. TOP OF ROD AND GROUND WIRE TO BE BELOW FROST LINE.
- CONTRACTOR SHALL COORDINATE INCOMING SERVICES WITH LOCAL UTILITIES PRIOR TO TRENCHING.
- ALL CONDUCTORS SHALL BE COPPER, 75 DEGREES C RATED, AND CONDUCTOR INSULATION BE THWN OR THHN.
- ALL TERMINATION SHALL BE LISTED AND IDENTIFIED FOR USE WITH 75°C RATED CONDUCTORS OPERATING AT 75°C.
- GROUND FAULT PROTECTION REQUIRED FOR UTILITY RECEPTACLES
- GENERATOR NEUTRAL SHALL NOT BE GROUNDED AT THE GENERATOR. REFER TO SINGLE LINE DETAIL, SHEET E-1.
- EQUIPMENT LOCATED OUTSIDE OR EXPOSED TO MOISTURE SHALL BE NEMA 3R RATED.
- CONTRACTOR SHALL USE SCHEDULE 80 PVC CONDUIT THROUGH CONCRETE AND ABOVE GROUND, UNLESS
- ALL NEWLY INSTALLED EQUIPMENT SHALL BE RATED "AT 10K AIC" MINIMUM. HIGHER RATINGS SHALL BE REQUIRED WHERE AVAILABLE FAULT CURRENT EXCEEDS THIS VALUE, EXACT FAULT CURRENT AVAILABLE SHALL BE COORDINATED WITH LOCAL UTILITY BASED ON EXACT CONDITIONS (XFMR SIZE, PERCENT IMPEDANCE, LENGTH OF





- GRADE

#2 AWG BCW

**GROUND ROD** 

%"Ø x 10'-0"

LONG MAX.

GROUND RING

18" OR 6" BELOW FROST

LINE, WHICHEVER IS

DEEPER, PLACED AS

APPROVED BY PG&E

GROUND RODS SHALL HAVE A MAXIMUM SPACING TWICE THE LENGTH OF ROD

GROUND RODS MAY BE:

SOLID COPPER

- COPPER CLAD STEEL

- SEE RESISTIVITY REPORT FOR VERIFICATION AS AVAILABLE
- A LARGER CONDUCTOR SHALL BE REQUIRED IN AREAS HIGHLY PRONE TO LIGHTNING AND/OR AREAS WITH HIGHLY ACIDIC SOIL
- GROUND RODS INSTALLED WITHIN CLOSE PROXIMITY TO TOWER OR WHEN SOIL IS AT OR BELOW 2,000 OHM-CM, SHALL BE GALVANIZED TO PREVENT GALVANIC CORROSION OF TOWER, (SEE ANSI/TIA-EIA-222)
- PROVIDE (1) GROUND LEAD TO EACH SIDE OF THE GENERATOR

#### **GROUND ROD DETAILS**

#### FENCE GROUNDING:

SEE FENCE & GATE DETAILS SHEET FOR ADDITIONAL

TYPICAL GROUNDING DIAGRAM

CONTRACTOR SHALL NOT SUBMIT BIDS OR PERFORM CONSTRUCTION WORK ON THIS PROJECT WITHOUT ACCESS TO THE CURRENT COMPLETE SET OF DRAWINGS LISTED IN THE TITLE-SHEET INDEX.

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GENERATOR INSTALLATION **PROJECT** 

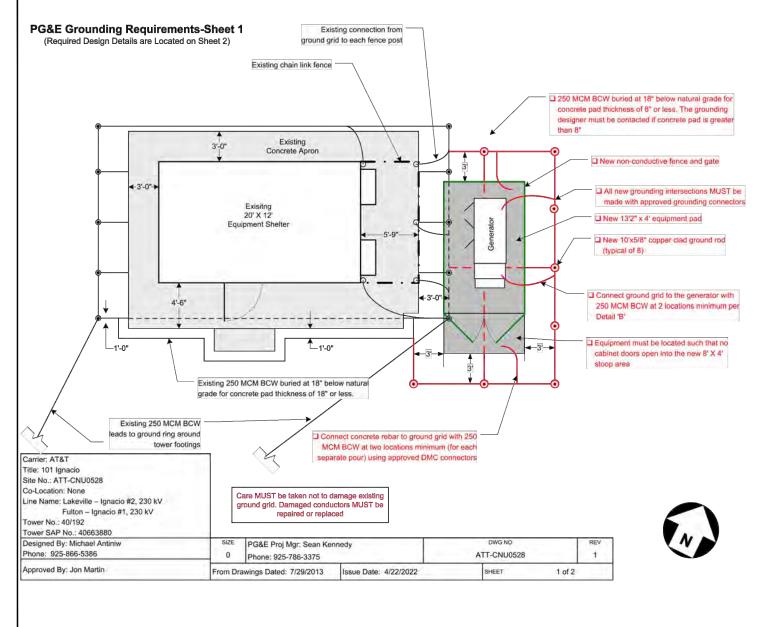
> 150 HAMILTON ROAD NOVATO, CA 94945

JURISDICTION USE

SHEET TITLE:

**ELECTRICAL DETAILS** 

SHEET NUMBER:



The following design details MUST BE incorporated into the final engineering and construction drawings for the cell site ground grid. Where conflicts arises between these details and cell vendor generic details, these details SHALL prevail.

#### **REQUIRED DESIGN DETAILS:**

- \_\_\_\_\_1. All grounding connections and grid intersections SHALL be made using approved 'DMC GroundLok System' compression components.
- 2. Ground grid safety calculations are based on the ground grid conductors being at 18" below natural grade with a concrete equipment pad of no more than 18" thick. Any pad thickness greater than 18" MUST be verified as acceptable by the grounding designer.
- \_\_\_\_\_3. All above ground metallic equipment SHALL be located fully within (3'-0" minimum) the concrete pad (including open doors and panels). Cable trays and conduits running outside the concrete pad MUST be non-metallic.
- 4. All concrete SHALL contain #4 rebar with a 1'-0" maximum grid spacing. All rebar intersections MUST be securely tied together. If concrete is poured in separate sections, each section must be connected to ground grid with 2-250 MCM BCW or equivalent.
- \_\_\_\_\_5. Coax ground MUST be connected to the ground grid with 2-250 MCM BCW or equivalent. If more than one ground bus is used, all ground buses must be either connected together or connected to ground grid separately with #2 BCW or larger.
- 6. Electric meter MUST be located fully within the boundary of the concrete pad. Any exception to this MUST be cleared through Michael Antiniw (925) 866-5386 prior to construction. Special service requirements may be required to isolate ground grid from other customer neutral wires.
- 7. Meter ground rod MUST be attached to the cell site ground grid with a 250 MCM BCW or equivalent.
- □\_\_\_\_\_8. Ground grid backfill material (at least 6") covering the 250 MCM BCW MUST be clean loamy material (or conductive material) and be free of rocks and foreign material.
- 9. If drilling is required to achieve ground rod depth, a minimum 2" hole is required. The hole MUST be backfilled with bentonite (or equivalent) material.
- □ \_\_\_\_\_10. Care MUST be taken not to damage existing ground grid. Damaged conductors MUST be repaired or replaced.
- 1\_\_\_\_\_12. Concrete pad size or any dimension stated on sheet 1 can not be changed without prior authorization from the grounding designer.

Title: 101 Ignacio Site No.: ATT-CNU0528 Co-Location: None Line Name: Lakeville - Ignacio #2, 230 kV Fulton - Ignacio #1, 230 kV Tower No.: 40/192 Tower SAP No.: 40663880 Designed By: Michael Antiniw PG&E Proj Mgr: Sean Kennedy Phone: 925-866-5386 ATT-CNU0528 Phone: 925-786-3375 Approved By: Jon Martin SHEET From Drawings Dated 7/29/2013 Issue Date: 4/22/2022 2 of 2

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GENERATOR INSTALLATION PROJECT

150 HAMILTON ROAD NOVATO, CA 94945

JURISDICTION USE

SHEET TITLE:

PG&E GROUNDING SPECIFICATIONS

SHEET NUMBER:



Report Date: 4/22/22

Revision:

### High Voltage Transmission Tower Cell Site Datasheet

#### Site Information

Company: AT&T

101 Ignacio Site name:

Site number: ATT-CNU0528

150 Hamilton Road, Novato Site address:

PG&E Contact: Michael Antiniw

Phone: (925) 866-5386

## Soil Data

Soil Model: Horizontal 4 layer

Top Layer

80.0 Ohm-meters

2.0 Feet 13.0 Feet

Middle 1 Middle 2 25.0 Ohm-meters 1.4 Ohm-meters

34.0 Feet

Bottom

12.0 Ohm-meters Infinite thickness

#### **GPR** Information

Grid Area Grid Resistance Ground Fault Duty

0.295 Ohms 16,231 Amps RMS

3,352 Ft2

X/R Ratio Voltage (Line-Line) 12.58 230 kV RMS

DC Offset

1.78

GPR RMS

4,787 Volts RMS

**GPR Peak Symmetrical** 

GPR Peak with DC Offset

6,771 Volts (Peak Symmetrical) 12,045 Volts (Peak Asymmetrical)

Michael Antiniw PG&E Representative 4/22/2022



#### Electric Power Station High Voltage Datasheet

#### Station Information

Station Name: Ignacio

Site address: Hamilton Dr. and Bel Marin Keys, Ignacio, CA

PG&E Contact: Tim Kintanar

Phone: (925) 866-5868

#### Soil Data

Soil Model: Horizontal 3 layer

> 55.00 Ohm-meters Top Layer

2.50 Feet

Report Date: 1/25/18

Revision:

Middle Bottom

5.00 Ohm-meters 42.00 Ohm-meters

40.00 Feet Infinite thickness

#### **GPR** Information

Grid Area 371,010 Ft2 Grid Resistance 0.074 Ohms Ground Fault Duty

X/R Ratio

13,309 Amps RMS 12.6

Voltage (Line-Line) DC Offset

230 kV RMS 1.78

GPR RMS

741 Volts RMS

**GPR Peak Symmetrical** GPR Peak with DC Offset 1,048 Volts (Peak Symmetrical) 1,864 Volts (Peak Asymmetrical)

Tim Kintanar PG&E Representative

1/25/2018

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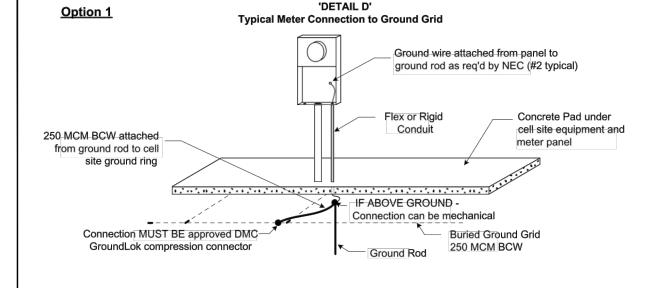
> 150 HAMILTON ROAD NOVATO, CA 94945

SHEET TITLE:

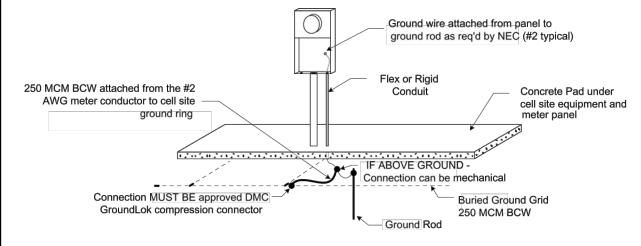
**PG&E GROUNDING SPECIFICATIONS** 

SHEET NUMBER:

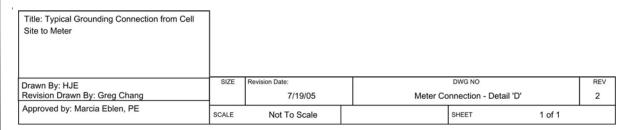
#### Connection Detail "B"

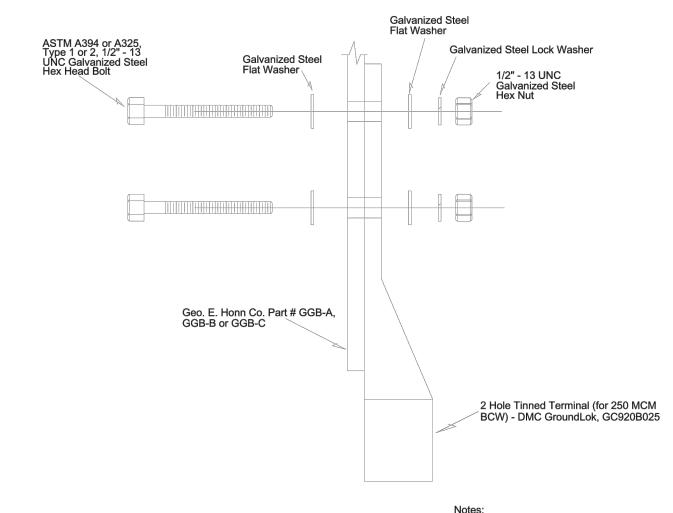


#### Option 2



\_\_\_\_\_\_





## Reference Drawings:

Sheet 1 Arrangement Sheet 2 Ground Bar Details Sheet 3 Bolting Detail "A" Sheet 5 Installation Guide

# \_

- Coat any cut or drilled surfaces with cold galvanizing compound.
   Clean area on flat bar where connector is to be to be the drilled with a wire bare.
- Clean area on hat par where connector is to be bolted with a wire brush. Use Penetrox "A" or equivalent as a coating between connector and tower leg.
- 3. All bolting material per ASTM A 394 or A325, Type 1 or 2. Bolts to be torqued to 480 in/lbs.
- 4. After installation and torquing, center punch the bolt threads in at least one location at the Hex Nut interface.

Title: Theft Deterrent Tower Ground Bolting Detail 'B'			'	ocation at the	nex Nut interio	ace.	
Drawn By: Bill DeHart	SIZE	Revision Date:			DWG NO		REV
Revision Drawn By: Steve Maddix	0	7/29/	09				3
Approved By: Marcia Eblen	SCALE	none			SHEET	4 of 5	

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GENERATOR INSTALLATION
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150 HAMILTON ROAD NOVATO, CA 94945

JURISDICTION USE:

SHEET TITLE:

PG&E GROUNDING SPECIFICATIONS

SHEET NUMBER:

INDUSTRIAL DIESEL GENERATOR SET

GENERAC | INDUSTRIAL

EPA Certified Stationary Emergency

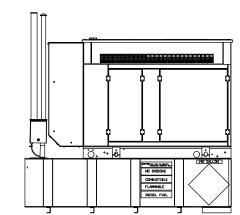
Standby Power Rating 30 kW, 38 kVA, 60 Hz

Prime Power Rating\* 27 kW, 34 kVA, 60 Hz





\*EPA Certified Prime ratings are not available in the US or



#### Codes and Standards

Not all codes and standards apply to all configurations. Contact factory for details.



UL2200, UL508, UL489, UL142, UL-2085



CSA C22.2



BS5514 and DIN 6271



**SAE J1349** 



NFPA 37, 70, 99, 110



NEC700, 701, 702, 708



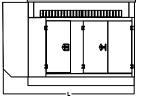
ISO 3046, 7637, 8528, 9001

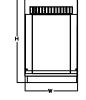


NEMA ICS10, MG1, 250, ICS6, AB1



ANSI C62.41





# Powering Ahead

For over 50 years, Generac has provided innovative design and superior manufacturing.

Generac ensures superior quality by designing and manufacturing most of its generator components, including alternators, enclosures and base tanks, control systems and communications software.

Generac gensets utilize a wide variety of options, configurations and arrangements, allowing us to meet the standby power needs of practically every application.

Generac searched globally to ensure the most reliable engines power our generators. We choose only engines that have already been proven in heavy-duty industrial applications under adverse conditions.

Generac is committed to ensuring our customers' service support continues after their generator purchase.

#### LEVEL 2 ACOUSTIC ENCLOSURE

Run Time	Usable Capacity	L x W x H - in (mm)		t - lbs (kg) sure Only
- Hours	- Gal (L)		Steel	Aluminun
No Tank	-	94.8 (2,407) x 38.0 (965) x 61.1 (1,551)	)	
19	54 (204)	94.8 (2,407) x 38.0 (965) x 74.1 (1,881)	)	0.44
47	132 (501)	94.8 (2,407) x 38.0 (965) x 86.1 (2,186) 94.8 (2,407) x 38.0 (965) x 98.1 (2,491)	510	341 (155)
75	211 (799)	94.8 (2,407) x 38.0 (965) x 98.1 (2,491)	(232)	(100)
107	300 (1,136)	94.8 (2,407) x 38.0 (965) x 98.1 (2,491)	)	

<sup>\*</sup> All measurements are approximate and for estimation purposes only. Specification characteristics may change without notice. Please contact a Generac Power Systems Industrial Dealer for detailed installation drawings

**EPA Certified Stationary Emergency** 

#### STANDARD FEATURES

#### **ENGINE SYSTEM**

- · Oil Drain Extension
- · Air Cleaner
- Fan Guard
- · Stainless Steel Flexible Exhaust Connection
- · Factory Filled Oil and Coolant
- · Radiator Duct Adapter (Open Set Only)
- Critical Silencer (Enclosed Unit Only)
- · Engine Coolant Heater

#### **Fuel System**

- · Fuel Lockoff Solenoid
- · Primary Fuel Filter

#### Cooling System

· Closed Coolant Recovery System

• 50/50 Ethylene Glycol Antifreeze

- UV/Ozone Resistant Hoses
- · Factory-Installed Radiator
- · Radiator Drain Extension

# **Electrical System**

· Battery Charging Alternator

**CONTROL SYSTEM** 

**Program Functions** 

· Programmable Crank Limiter

• 7-Day Programmable Exerciser

• RS-232/485 Communications

· Isochronous Governor Control

· Waterproof/Sealed Connectors

· 2-Wire Start Capability

- · Battery Cables
- · Battery Tray
- Rubber-Booted Engine Electrical Connections

Digital H Control Panel- Dual 4x20 Display

Special Applications Programmable Logic Controller

· All Phase Sensing Digital Voltage Regulator

• Date/Time Fault History (Event Log)

 $\odot$ 

· Solenoid Activated Starter Motor

#### **ALTERNATOR SYSTEM**

- UL2200 GENprotect
- · Class H Insulation Material
- 2/3 Pitch
- Skewed Stator
- · Brushless Excitation
- · Sealed Bearing
- Rotor Dynamically Spin Balanced
- · Amortisseur Winding (3-Phase Only)
- Full Load Capacity Alternator
- · Protective Thermal Switch

#### **GENERATOR SET**

- · Internal Genset Vibration Isolation
- · Separation of Circuits High/Low Voltage
- · Separation of Circuits Multiple Breakers Wrapped Exhaust Piping
- Standard Factory Testing
- 2 Year Limited Warranty (Standby Rated Units)
- 1 Year Limited Warranty (Prime Rated Units)
- Silencer Mounted in the Discharge Hood (Enclosed Unit Only)

#### NOTE: IT IS RECOMMENDED THAT BATTERY BE WITHIN LEAK CONTAINMENT BOX OR TRAY

· Audible Alarms and Shutdowns

• E-Stop (Red Mushroom-Type)

Predictive Maintenance Algorithm

16 Channel Remote Trending

**Full System Status Display** 

· kW Hours, Total, and Last Run

· Real/Reactive/Apparent Power

Password Parameter Adjustment Protection

• 0.2 msec High Speed Remote Trending

Alarm Information Automatically Annunciated

· Not in Auto (Flashing Light)

· Auto/Off/Manual Switch

Modbus<sup>®</sup>Protocol

Single Point Ground

on the Display

· Power Output (kW)

· All Phase AC Voltage

· All Phase Currents

Power Factor

Sealed Boards

#### **ENCLOSURE (If Selected)**

· Rust-Proof Fasteners with Nylon Washers to Protect Finish

INDUSTRIAL

- · High Performance Sound-Absorbing Material (Sound Attenuation Enclosures)
- · Gasketed Doors

GENERAC

- · Stamped Air-Intake Louvers
- Upward Facing Discharge Hoods
- (Radiator and Exhaust) · Stainless Steel Lift Off Door Hinges
- · Stainless Steel Lockable Handles
- RhinoCoat Textured Polyester Powder Coat Paint

#### **FUEL TANKS (If Selected)**

- UL-2085
- · Double Wall
- Normal and Emergency Vents
- Sloped Top
- Sloped Bottom · Factory Pressure Tested
- · Rupture Basin Alarm
- Fuel Level
- · Check Valve In Supply and Return Lines
- · RhinoCoat- Textured Polyester Powder Coat Paint
- · Stainless Steel Hardware

#### · Oil Pressure

- · Coolant Temperature
  - · Coolant Level
- · Engine Speed • NFPA110 Level I and II (Programmable) · Battery Voltage
- · Customizable Alarms, Warnings, and Events Frequency

### Alarms and Warnings

- Oil Pressure
- · Coolant Temperature
- · Coolant Level
- · Engine Overspeed
- · Battery Voltage

Alarms and Warnings

- Alarms and Warnings Time and Date Stamped Snap Shots of Key Operation Parameters During
- Alarms and Warnings Spelled Out (No Alarm Codes)

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**GENERAC 30KW GENERATOR SPECIFICATIONS** 



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HWY 101 - IGNACIO

10088152 GENERATOR INSTALLATION

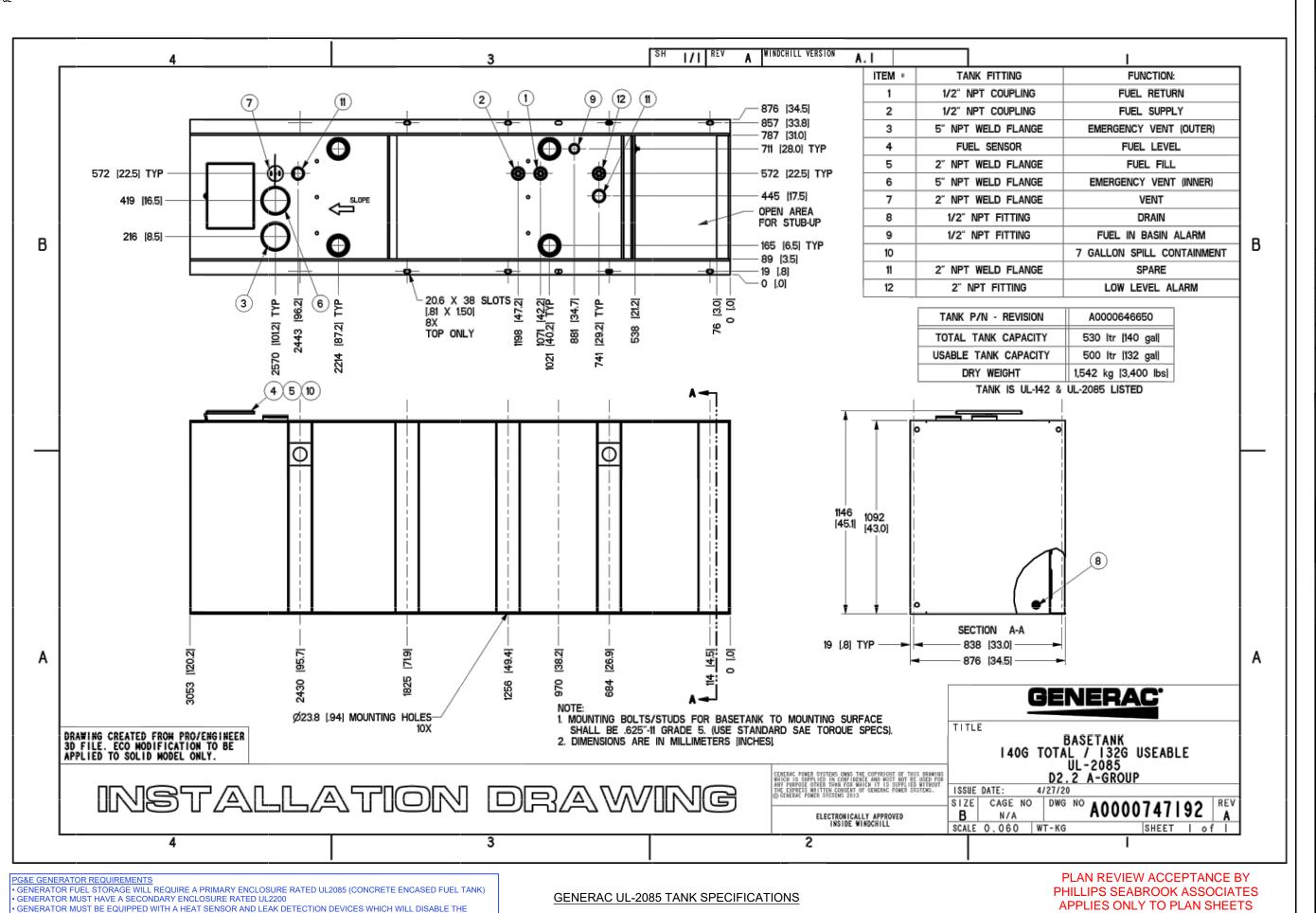
> **PROJECT** 150 HAMILTON ROAD NOVATO, CA 94945

JURISDICTION USE:

SHEET TITLE:

**GENERATOR SPECIFICATIONS** 

SHEET NUMBER:



GENERATOR IN CASE OF FUEL LEAKAGE, FIRE, OR OTHER EXTERNAL CIRCUMSTANCES

GENERATOR MUST HAVE A FIRE DETECTION SHUT-OFF VALVE

WHICH HAVE THIS STAMP



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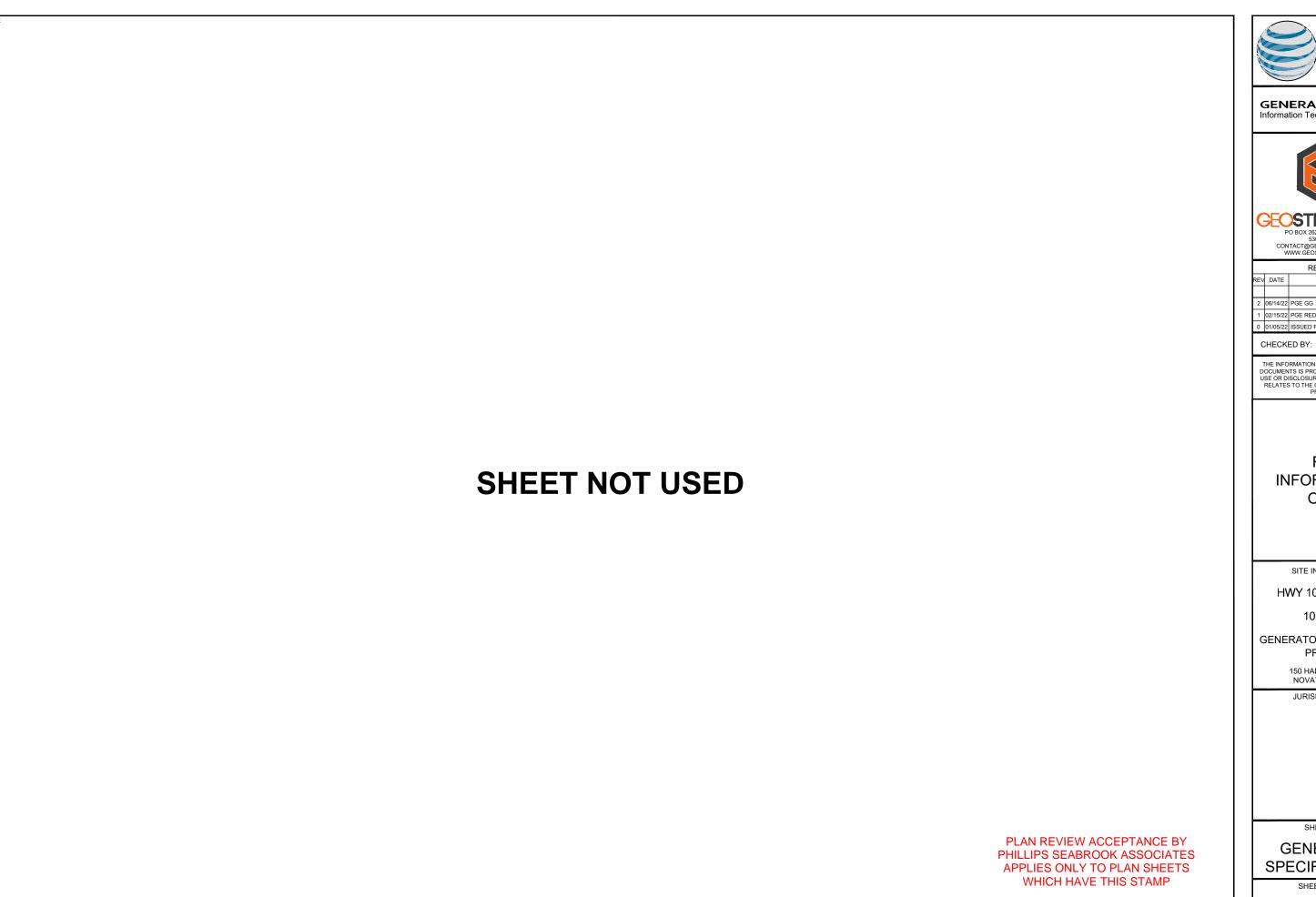
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GENERATOR INSTALLATION PROJECT

150 HAMILTON ROAD NOVATO, CA 94945

JURISDICTION USE:

SHEET TITLE:

GENERATOR SPECIFICATIONS

SHEET NUMBER:

#### EXPLODED VIEW: EV VENT EXT AGRP 2"3 ATT

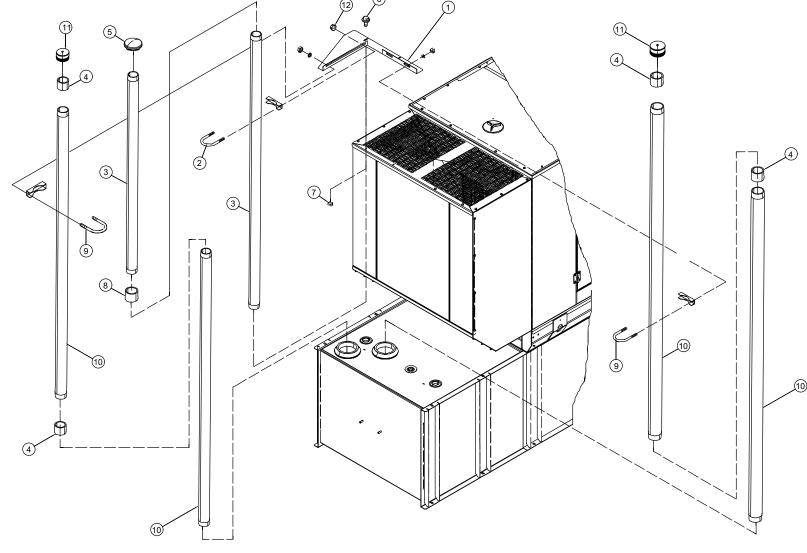
#### DRAWING #:0K9817A

# **GROUP H**

ITEM	PART#	QTY.	DESCRIPTION
(1)1	0G3036YST0R	1	BRACKET VENT EXT AGRP 2"3 ATT
`ź	0C7947	1	KIT, SADDLE AND BOLT 2 1/2"
3	0G3045	2	PIPE 2"VENT EXTENSION 72"LG
4	10000016676	4	COUPLING PIPE 3 ZINC
5	G021178	1	VENT OEM 2"
6	0C2454B	2	SCREW HWHT M6-1 X 30 W/MKS
7	G049813	2	NUT HEX M6-1.0 G8 CLEAR ZINC
8	068640B	1	COUPLING FULL 2-11.5 BLACK
9	0E4264	2	BOLT U 3/8-16 X 3.50" W/SADDLE
10	0H1454	4	PIPE NIPPLE 3"X72" SCH40 PNTBK
11	072989J	2	VENT CAP EMERG 3"NPT
12	G064101	2	NUT HEX FL WHIZ 3/8-16

#### NOTES (UNLESS OTHERWISE SPECIFIED)

- (1) SHEET METAL PARTS LISTED IN THE BOM TABLE ARE REPRESENTING CENERIC PARTS (NO COLOR).
- \* MANUFACTURING: FOR CORRECT MATERIAL AND COLOR REFER TO AS400 BOM.
  \* CUSTOMER: WHEN ORDERING REPLACEMENT PARTS, ENTER BASE NUMBER
- \* CUSTOMER: WHEN ORDERING REPLACEMENT PARTS, ENTER BASE NUMBER
  (FIRST 6 DIGITS ONLY) IN THE SYSTEM FOR CORRECT MATERIAL AND COLOR. (FOR REFERENCE SEE

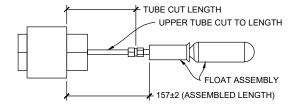


REVISION : CN-0019649-W DATE ; 9/4/18 **EMERGENCY VENT PIPE ASSEMBLY** 

EXPLODED VIEW : EV VENT EXT AGRP 2"3 ATT DRAWING NO. : 0K9817A

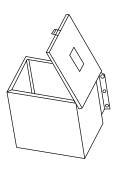
#### GENERAC GENERATOR SPECIFICATIONS

## OVERFILL PREVENTION VALVE INSIDE TANK (FACTORY-INSTALLED)



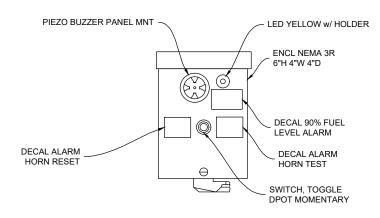
GENERAC 0J7671

#### FUEL SPILL/FILL DRAIN OUTSIDE TANK (FACTORY-INSTALLED)



GENERAC 0J7606A

## REMOTE 90% FUEL ALARM (FACTORY-INSTALLED)



#### GENERAC OF2908\$

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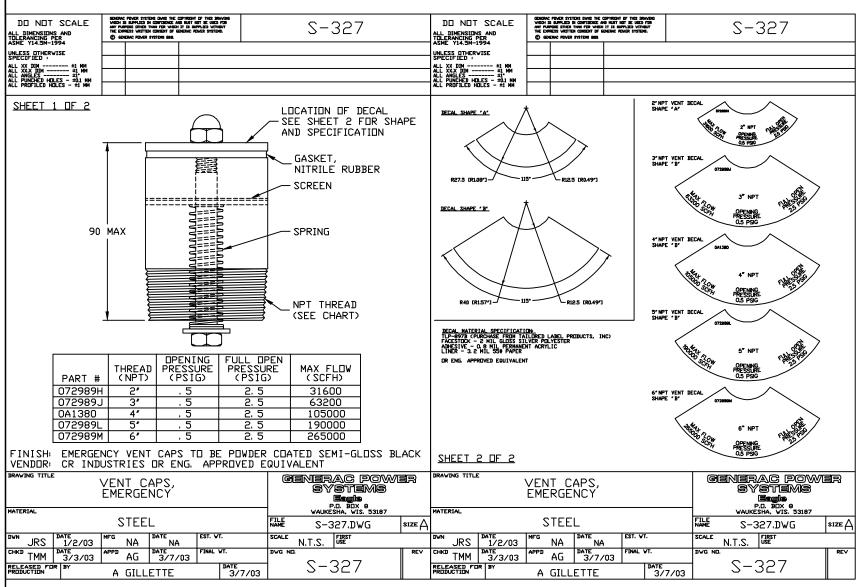
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SHEET TITLE:

GENERATOR SPECIFICATIONS

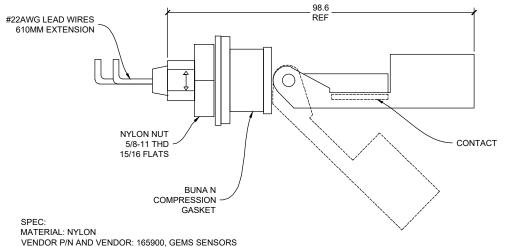
SHEET NUMBER:



**GENERAC EMERGENCY VENT CAPS** 

#### FUEL LEAK DETECTOR ALARM (FACTORY-INSTALLED)

INSTALLATION NOTE: HAND TIGHTEN + ONE QUARTER TURN. LEAK DETECTION MUST BE INSTALLED IN THE NORMALLY OPEN (N.O.) POSITION AS SHOWN FOR IT TO FUNCTION CORRECTLY IN GENERAC'S UL TANK SECONDARY CONTAINMENT LEAK DETECTION APPLICATION. OVER TIGHTENING WILL RESULT IN DAMAGE TO THE LEAK DETECTOR AND IMPROPER OPERATION.



MOUNTING ATTITUDE: HORIZONTAL RECOMMENDED HOLE SIZE: Ø 0.875", 1/32"-5/32" THICK PANEL OPERATING TEMPERATURE: -40°F TO 250°F MAX. OPERATION PRESSURE: 100 PSIG AT 70°F THIS SWITCH IS U.L. RECOGNIZED - FILE #E45168, CSA LISTED - 30200 CONTACT RATING: 0.17 AMP, 120 V, 60 Hz, RESISTIVE 0.08 AMP, 240 V, 60 Hz, RESISTIVE

20 VA PILOT DUTY

DC ELEC. RATING: 0.3 AMP MAX @30 VDC

GENERAC 096500B

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GENERATOR INSTALLATION **PROJECT** 

> 150 HAMILTON ROAD NOVATO, CA 94945

JURISDICTION USE:

SHEET TITLE:

**GENERATOR SPECIFICATIONS** 

SHEET NUMBER:

TTS Series
Switches



200 Amps 600 VAC

**TAS200** 

200A Automatic Transfer Switch

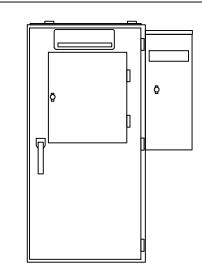
The Generac TAS200 Automatic Transfer Switch

Flexibility for multiple application installations

Multiple generator support with 3 source panel

Designed with a 6 inch touch screen controller for improved user interface

Camlock functionality for mobile generator sources



#### **Features**

- = STEEL CONSTRUCTION
- NEMA 3R ENCLOSURE WITH HINGED "PADLOCKING" DOORS
- = STAINLESS STEEL HARDWARE
- = CAMLOCK "QUICK CONNECT" CAPABILITY
- OPERATIONAL STATUS VIEW VIA 6 INCH TOUCH SCREEN
- = TEST FUNCTION FAST TEST & NORMAL TEST
- = UL1008 LISTED FOR EMERGENCY SYSTEMS

# **Optional Features**

- = EXTENDED WARRANTY
- = THREE-PHASE VOLTAGE CONFIGURATIONS

#### **Codes and Standards**

Generac products are designed to the following standards:



UL1008, UL508, UL50, CSA C22.2 No. 178



NEC 700, 701 and 702



**NEMA 250** 

# Application and Engineering Data

Cabinet Specifications				
<u>Dimensions</u> 24"W x 12"D x 48"H				
Weight	210 lbs.			
	Single Chamber with Main Door			
	Steel			
	UL Type / NEMA 3R Rated			
Construction	Powder Coat Finish for Corrosion Resistance			
	C-UL-US Listed - Automatic Transfer Switch			
	Stainless Steel Hardware			
	3-Point Latching System with Pad-Lockable Handles			
Mounting Ontions	Wall			
Mounting Options	H-frame			
Installed Pre-wired alarm terminal strip				

Electrical Specifications				
Voltage/Phase/Amps	120/240 Single-Phase, 200A 120/208 3-Phase, 200A 120/240 3-Phase, 200A			
Breaker	Eaton 200 amp Utility Breaker			
bieakei	Eaton 200 amp Generator Breaker			
Maximum RMS Symmetrical Fault Current - Amps	25k AIC Rated			
Protective Device Continuous Rating (Max) Amp	200			
Input to Generator	350MCM - #6 AWG			
Output to Site	350MCM - #6 AWG			
Generator Annunciator Connector	Deutsch DTM04-12PA-L012			
	Generator Run Alarm			
	Generator Fail - Shutdown Alarm			
Alama Tamain al Danad	Generator Fail - Non Shutdown Alarm			
Alarm Terminal Board	Low Fuel Alarm			
	Generator Theft Alarm			
	AC Utility Fail Alarm			

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GENERATOR INSTALLATION PROJECT

150 HAMILTON ROAD NOVATO, CA 94945

JURISDICTION USE:

SHEET TITLE:

ATS SPECIFICATIONS

SHEET NUMBER:

E-5.0



# TTS Control Systems

#### INDICATORS AND BUTTONS

Ī	. System Ready indicator	. Normal Test button
	. Standby Operating indicator	. Fast Test button
	. Utility Available indicator	. Return to Normal button
	. GEN/UTIL Switch Position indicator	. Reset button
	. TVSS status	. Exercising indicator

#### **DETAILS SCREEN**

System Settings:  . System Voltage/Phases:	Exercise Settings:  . Time of day . Day of week . Exercise:  - Exercise with/without load - Exercise once every 1, 2, or 4 weeks Exercise time-of-day - Exercise day of week - Exercise duration: 15-30 minutes
- Delay time: 0-60s . Utility Interrupt Delay: 0-60s . Return to Utility Timer: 1-30 minutes . Transfer: - In-phase, or - Time-Delay-Neutral at 0.0-10.0s in 1 second increments	Screen Settings: . Brightness & Contrast button . Screen Calibration button . Startup/Clean screen
increments	Diagnostics:
Engine Settings:	. Digital I/O bits status . Voltage A/D readings
Engine Warm-up timer: 0-20 minutes     Generator Load Accept:     - Time-Delay-Neutral at 0.0-10.0s in 1 sec increments     - Voltage: 85-95% of nominal     - Frequency: 85-95% of nominal     Engine Minimum Run Timer: 5-30 minutes     Engine Cooldown Timer: 0-20 minutes	Mimic Diagram: . System Ready . Transfer switch position . Utility available . Standby available . Maintenance/Auto switch position . Generator source TS position . TVSS status

Camlock Component				
Camlock Component	Shipped loose for multiple installation options			
Dimensions	9" W x 9.4" D x 24.25" H			
	Single-Phase: Black L1, Red L2, White-Neutral, Green-Ground			
200A Camlock Generator Connection	3-Phase: Black L1, Red L2, Blue L3, White-Neutral, Green-Ground			
200A Calliock Generator Connection	Uses 4 CH E1016 Male Connectors			
	Mating Connector - CH E1016 Female			

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150 HAMILTON ROAD NOVATO, CA 94945

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SHEET TITLE:

CAM-LOCK BOX SPECIFICATIONS

SHEET NUMBER:

E-5.1



# **GENERAL DYNAMICS**

Information Technology

# **CITY OF NOVATO**



# **Structural Analysis Report**

New Concrete Slab •

Site ID: 10088152

Site Name: Hwy 101 - Ignacio
Project: Generator Upgrade

Prepared For: AT&T

Structure Description: Concrete Slab & Anchorage

**Diesel Backup Generator** 

Site Location: 150 Hamilton Road

**Novato, CA 94945** 

**Marin County** 

38.078248°, -122.541598°

Design Codes: CBC 2019

IBC 2018 w/ State Amendments

**ASCE 7-16** 



September 13 2022 PHILLIPS SEABROOK ASSOCIATES

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Revision 1 February 15, 2022

Date Signed: 2/15/2022

10088152\_Gen Slab Analysis\_R1 220215 3996

#### 1.0 Introduction

GeoStructural has completed a structural analysis for the existing AT&T 10088152 communications site located in Marin County, CA. The scope of this structural analysis is limited to the following:

- 9'-2" x 15'-0" x 6" Reinforced Concrete Generator Slab w/ #4 Bars @ 12" 0.C. Each Way & 1'-9" Turndown Edges w/ (2) #4 Horiz and #4 Hooks @ 12" o.c..
- Generac UL2085 Diesel Generator Equipment Anchorage.

The existing communications structure/foundation and existing equipment platform(s)/shelter(s) are designed by others and beyond the scope of this analysis.

#### 2.0 Analysis & Design Criteria

This analysis is pursuant to the following design criteria:

- CBC 2019 California Building Code.
- IBC 2018 International Building Code.
- ASCE 7-16 Minimum Design Loads and Associated Criteria for Buildings and Other Structures.
- AISC Steel Construction Manual.
- ACI 318-14 Building Code Requirements for Structural Concrete.

Gravity Design Loading:				
Generac UL2085 30kW Generator w/ L2	Generac UL2085 30kW Generator w/ L2A Enclosure = 2,182lbs			
132gal Fuel Tank(Dry) = 3200 lbs				
Diesel Fuel (100% Fill + 35% Contain) = $7$	7.3 lb/gal(178gal) = 1300 lbs			
WET Total Assembly Weight = 6.683 kips	; DRY Total Assembly Weight = 5.382 kips			
Wind Design Loading:				
Design Wind w/o ice = 92 mph [3-sec gust Ultimate ASCE Figure 26.5-1B]				
Exposure Category C Topographic Category 1				
Risk Category II				
Seismic Design Loading:				
Site Class D Importance Factor, I <sub>p</sub> = 1.0				
$S_s = 1.500, S_1 = 0.600, S_{DS} = 1.200$				

All data required to complete our structural analysis was furnished by our client. GeoStructural has <u>not</u> conducted an independent study to verify existing site conditions and the results of this analysis are based solely on the information provided.



# 3.0 Load Generation & Material Strength

#### Table 3.1 - Wind Design Loading

Wind Load - Velocity Pressure	ASCE 7-16, §29.3
$q_z = 0.00256 \ K_z \ K_{zt} \ K_d \ V^2$	Eq. 29.3-1
$K_z = 0.85$	Table 29.3-1
$K_{zt} = 1.00$	§ 26.8.2
$K_d = 0.90$	Table 26.6-1
V = 92 mph	Figure 26.5
$q_z = 0.00256*0.85*1.00*0.90*(92^2)/1000 = 0.0166 \text{ ksf}$	Eq. 29.3-1
Wind Load - Other Structures (Tanks & Similar Structures)	ASCE 7-16, §29.5
$F = q_z G C_f A_f$	Eq. 29.5-1
G = 0.85	§ 26.9
$C_f = 1.32$	Figure 29.5-1
Af = 77.6 ft2 Worst Case; 25.4 ft <sup>2</sup> Transverse (Side)	Generac UL2085
$F_N = 0.0166*0.85*1.32*77.6 = 1.44 \text{ kip};  F_T = 0.0166*0.85*1.32*25.4 = 0.47 \text{ kip}$	Eq. 29.5-1

## <u>Table 3.2 - Seismic Design Loading - 100% Fill + 35%</u>

Seismic Load - Non-Structural Components	ASCE 7-16, Chapter 13
$F_p = 0.4a_p S_{DS} W_p \{ (1+2(z/h)) / (R_p/I_p) \}$	Eq. 13.3-1
$F_p \le 1.6 S_{DS} I_p W_p$	Eq. 13.3-2
$F_p > 0.3 S_{DS} I_p W_p$	Eq. 13.3-3
Reversible Vert Force, $E_v = 0.2S_{DS}W_p = 0.2*1.200*6.683 = 1.60 \text{ kip}$	§ 13.3.1
$a_p = 1.0$	Table 13.6-1
$S_{DS} = (2/3)S_{MS} = 1.200$ ; $S_{D1} = (2/3)S_{M1}$	Eq. 11.4-3 & 4
Ss; S1	USGS Reference
Fa; Fv	Tables 11.4-1 & 2
$S_{MS} = F_a S_s$ ; $S_{M1} = F_v S_1$	Eq. 11.4-1 & 2
$W_p = 6.683 \text{ kip (Wet Weight)}$	From Section 2.0 Above
z = 2 ft (Conservative Anchorage Height of Generator to Tank Top)	Slab-On-Grade
h = 8.03 ft (Overall Height of Generator with Tank Assembly)	Slab-On-Grade
$R_p = 2.5$	Table 13.6-1
Importance Factor, Ip = 1.0	§ 11.5.1 & 13.1.3
$\rho$ = 1.0 (Exception from $\rho$ = 1.3, Non-Structural Components)	§ 12.3.4.2 & § 13.3.1
$F_p = 0.4a_p S_{DS} W_p \{ (1+2(z/h)) / (R_p/I_p) \}$ = 0.4*1.0*1.200*6.683*(1+2*(2/8.03))/(2.5/1.0) = 1.28 kip	Eq. 13.3-1
$F_p \le 1.6 S_{DS} I_p W_p = 1.6^* 1.200^* 1.0^* 6.683 = 12.83 \text{ kip}$	Eq. 13.3-2
$F_p > 0.3 S_{DS} I_p W_p = 0.3^* 1.200^* 1.0^* 6.683 = 2.41 \text{ kip}$	Eq. 13.3-3



Table 3.3 - Seismic Design Loading - 0% Fill

Seismic Load - Non-Structural Components	ASCE 7-16, Chapter 13
Reversible Vert Force, $E_V = 0.2 S_{DS} W_p = 0.2*1.200*5.382 = 1.29 \text{ kip}$	§ 13.3.1
$a_p = 1.0$	Table 13.6.1
$S_{DS} = (2/3)S_{MS} = 1.200$ ; $S_{D1} = (2/3)S_{M1}$	Eq. 11.4-3 & 4
Ss; S1	USGS Reference
Fa; Fv	Tables 11.4-1 & 2
$S_{MS} = F_a S_s$ ; $S_{M1} = F_v S_1$	Eq. 11.4-1 & 2
$W_{\rho} = 5.382 \text{ kip (Dry Weight)}$	From Section 2.0 Above
z = 2 ft (Conservative Anchorage Height of Generator to Tank Top)	Slab-On-Grade
h = 8.03 ft (Overall Height of Generator with Tank Assembly)	Slab-On-Grade
$R_p = 2.5$	Table 13.6.1
Importance Factor, Ip = 1.0	§ 11.5.1 & 13.1.3
$\rho$ = 1.0 (Exception from $\rho$ = 1.3, Non-Structural Components)	§ 12.3.4.2 & § 13.3.1
$F_p = 0.4a_p S_{DS} W_p \{ (1+2(z/h)) / (R_p/l_p) \}$ = 0.4*1.0*1.200*5.382*(1+2*(2/8.03))/(2.5/1.0) = 1.03 kip	Eq. 13.3-1
$F_p \le 1.6 S_{DS} I_p W_p = 1.6^* 1.200^* 1.0^* 5.382 = 10.33 \text{ kip}$	Eq. 13.3-2
$F_p > 0.3S_{DS}I_pW_p = 0.3*1.200*1.0*5.382 = 1.94 \text{ kip}$	Eq. 13.3-3

Table 3.4 - Seismic Overstrength Anchorage Loading (ACI 318-14 § 17.2.3.4.3(d) & 17.2.3.5.3(c))

Seismic Load - Non-Structural Components	ASCE 7-16, Chapter 13
$(0.9-0.2(S_{DS}))D + \Omega_0Q_E$	Eq. 12.4.3.2 (7)
$\Omega_0 = 2.5$	Table 13.6-1
Net OTM = (6.66*2.5)-(((0.9-(0.2*1.200))* 6.683)*1.5) = 10.04 k-ft	
Omega AB Tension = (10.0/(33/12)/(10/2))+((1.60*2.5)/10) = 1.13 kip	
Net Shear = (2.41*2.5)-(((0.9-(0.2*1.200))* 6.683)*0.3) = 4.69 kip	
Omega AB Shear = $4.69/(10/2) = 0.94$ kip (Assume only $1/2$ AB engage)	

Table 3.5 - Structural Component Material Strengths

Structural Component	Nominal Strength/Material <sup>1</sup>	
Mechanical Anchors	HILTI KWIK Bolt TZ2 Stainless Steel Expansion Anchors (ICC-ES ESR-4266)	
Concrete Slab	f <sub>c</sub> ' = 2500 psi	
Steel Reinforcing	F <sub>y</sub> = 60 ksi	
Allowable Soil Capacities	Bearing = 1,000 psf Passive Sliding = 100 psf/ft  µ = 0.3	

Strengths listed were utilized for this analysis and are based upon ASTM, AISC, RCSC, MSJC, AWS and ACI preferred specification values. Values and materials are consistent with industry standards. Material strengths were taken from original design documents, geotechnical reports, etc. when available.



## Table 3.6 - Analysis Parameter Design Checks

Parameter	Site Specific (Demand) <sup>1</sup>	6" Analysis (Allowable)¹	Result <sup>2</sup>
Concrete Strength (f'c)	2500	2500	
Anchor Tension	1.13	2.38	Adequate
Anchor Shear	0.94	1.84	

The analysis (allowable) values listed for each parameter are the minimum values required to safely transmit the imparted loading through the foundation and anchorage to the surrounding soil without creating an unstable condition. The allowable values are based on the minimum presumptive values shown in Table 3.5 above.



<sup>2.</sup> Since the site-specific individual demand parameters are less than or equal to the maximum allowable values listed the foundation and anchorage design is deemed adequate to support the loading.

#### 4.0 Conclusion & Recommendations

AT&T's proposed reinforced concrete slab-on-grade and generator mechanical anchorage will satisfy the requirements of the applicable design codes and have sufficient capacity to support the proposed backup diesel generator loading considered in this analysis.

- Reinforced Concrete Generator Slab:
  - 9'-2" x 15'-0" x 6" Reinforced Concrete Generator Slab w/ #4 Bars @ 12" O.C. Each
     Way & 1'-9" Turndown Edges w/ (2) #4 Horiz and #4 Hooks @ 12" o.c..
- Generac Diesel Generator Equipment Anchorage:
  - (10) 5/8"Ø x 3-3/4" Embed HILTI Kwik Bolt TZ2 stainless steel expansion anchors (ICC-ES ESR-4266 report).

#### Analysis Notes & Assumptions:

- All data required to complete our structural analysis was furnished by our client. GeoStructural has
   not conducted a site visit or independent study to verify existing conditions and the results of this
   analysis are based solely on the information provided.
- Proposed generator slab and anchorage shall be installed in accordance with any recommendations given in GeoStructural's approved Construction Drawings.

If any of the existing or proposed conditions reported in this analysis are not properly represented, please contact our office immediately to request an amended report. We appreciate the opportunity to provide our structural engineering services to you. If you have any questions regarding the content of this structural analysis report, please don't hesitate to contact us.

Prepared by:

Jesse Drennen, PE 208.761.7986

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Reviewed and Approved by:

Don George, PE 208.602.6569

don.george@geostructural.com

# 5.0 Attachments, Calculations & Software Output

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#### Address:

No Address at This Location

## **ASCE 7 Hazards Report**

Standard: ASCE/SEI 7-16

Risk Category: <sup>Ⅱ</sup>

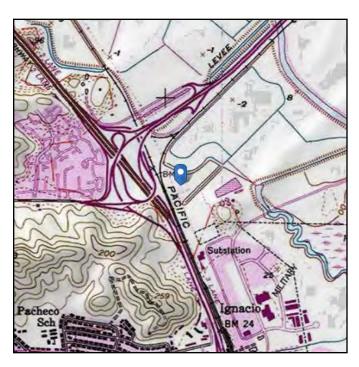
Soil Class: D - Default (see

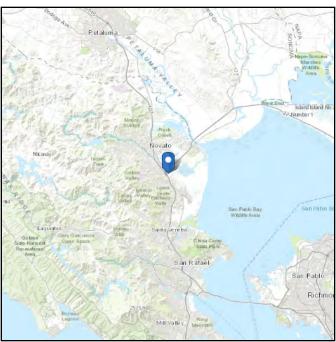
Section 11.4.3)

Elevation: 2.77 ft (NAVD 88)

Latitude: 38.078248

Longitude: -122.541598





## Wind

#### Results:

Wind Speed: 92 Vmph
10-year MRI 64 Vmph
25-year MRI 70 Vmph
50-year MRI 74 Vmph
100-year MRI 79 Vmph

Data Source: ASCE/SEI 7-16, Fig. 26.5-1B and Figs. CC.2-1–CC.2-4, and Section 26.5.2

Date Accessed: Mon Mar 22 2021

Value provided is 3-second gust wind speeds at 33 ft above ground for Exposure C Category, based on linear interpolation between contours. Wind speeds are interpolated in accordance with the 7-16 Standard. Wind speeds correspond to approximately a 7% probability of exceedance in 50 years (annual exceedance probability = 0.00143, MRI = 700 years).

Site is not in a hurricane-prone region as defined in ASCE/SEI 7-16 Section 26.2.



## **Seismic**

Site Soil Class: D - Default (see Section 11.4.3)

Results:

 $S_{\mbox{\scriptsize S}}$  :  $S_{\text{D1}}$  : 1.5 N/A  $T_L$ : S<sub>1</sub> : 12 0.6  $F_a$ : 1.2 PGA: 0.601  $F_v$ : N/A PGA<sub>M</sub>: 0.721  $S_{MS}$  :  $F_{PGA}$  : 1.8 1.2  $S_{M1}$ : N/A  $I_e$ : 1  $C_v$ :  $S_{\text{DS}}$  : 1.2 1.4

Ground motion hazard analysis may be required. See ASCE/SEI 7-16 Section 11.4.8.

Data Accessed: Mon Mar 22 2021

Date Source: <u>USGS Seismic Design Maps</u>



#### lce

#### Results:

Ice Thickness:0.00 in.Concurrent Temperature:25 FGust Speed:30 mph

**Data Source:** Standard ASCE/SEI 7-16, Figs. 10-2 through 10-8

Date Accessed: Mon Mar 22 2021

Ice thicknesses on structures in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

Values provided are equivalent radial ice thicknesses due to freezing rain with concurrent 3-second gust speeds, for a 500-year mean recurrence interval, and temperatures concurrent with ice thicknesses due to freezing rain. Thicknesses for ice accretions caused by other sources shall be obtained from local meteorological studies. Ice thicknesses in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.



## **Flood**

Results:

Flood Zone Categorization: AE

Base Flood Elevation: NAVD88

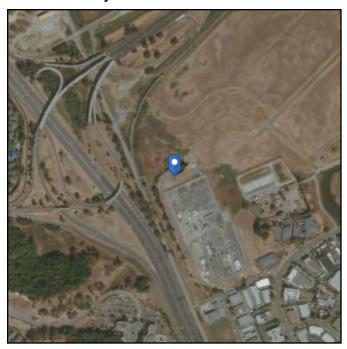
**Data Source:** FEMA National Flood Hazard Layer - Effective Flood Hazard Layer for US,

where modernized (https://msc.fema.gov/portal/search)

Date Accessed: Mon Mar 22 2021

FIRM Panel: If available, download FIRM panel here

**Insurance Study Note:** Download FEMA Flood Insurance Study for this area <a href="here">here</a>

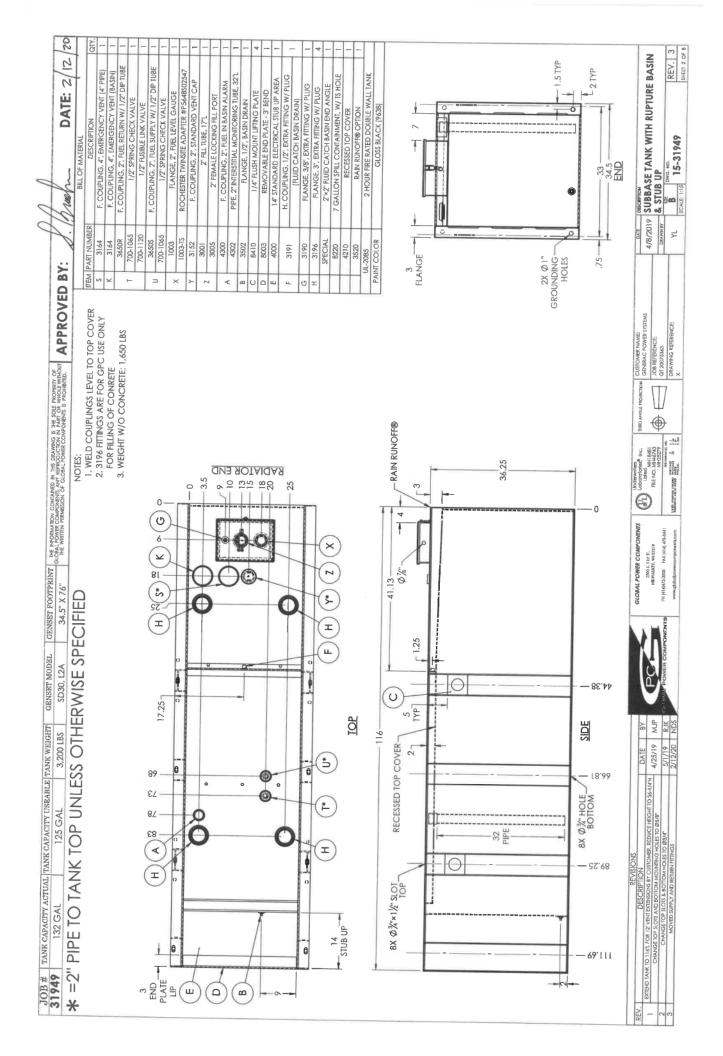




The ASCE 7 Hazard Tool is provided for your convenience, for informational purposes only, and is provided "as is" and without warranties of any kind. The location data included herein has been obtained from information developed, produced, and maintained by third party providers; or has been extrapolated from maps incorporated in the ASCE 7 standard. While ASCE has made every effort to use data obtained from reliable sources or methodologies, ASCE does not make any representations or warranties as to the accuracy, completeness, reliability, currency, or quality of any data provided herein. Any third-party links provided by this Tool should not be construed as an endorsement, affiliation, relationship, or sponsorship of such third-party content by or from ASCE.

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GeoStructural LLC PO Box 2621 Boise, ID 83701

Project Title: AT&T Generator Upgrade Project Engineer: Jesse Drennen, PE

Engineer: Project ID:

Project Descr: Standby Generator on Concrete Slab

## **Building Code Information**

 $File = E: \label{eq:File} File = File$ Software copyright ENERCALC, INC. 1983-2018, Build:10.18.12.30 .

Licensee: GeoStructural, LLC

Lic. # : KW-06009677

Governing Code: IBC 2018, ASCE 7-16, CBC 2019, AISC 360-16, NDS 2018, ACI 318-14, TMS City Jurisdiction: Contact Name: Alternate Contact: Building Official: Address:,,

Phone: Fax: eMail:

Notes:

GeoStructural LLC PO Box 2621 Boise, ID 83701

Project Title: AT&T Generator Upgrade Project Engineer: Jesse Drennen, PE

Engineer: Project ID:

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## **Project Information**

 $File = E: \label{eq:file} File = File$ Software copyright ENERCALC, INC. 1983-2018, Build:10.18.12.30 .

Licensee: GeoStructural, LLC

Lic. # : KW-06009677

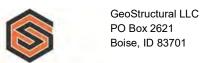
Project Title: AT&T Generator Upgrade Project Description: Standby Generator on Concrete Slab

I.D. : Address:,,CA

Project Leader : Jesse Drennen, PE

Phone: 208-761-7986 Fax: eMail:

**Project Notes** 



Project Title: Engineer:

AT&T Generator Upgrade Project

Jesse Drennen, PÉ

Project ID: Project Descr:

Standby Generator on Concrete Slab

## **GEOSTRUCTURAL**

## **General Footing**

LIC#: KW-06015027, Build:20.22.1.12 GeoStructural, LLC (c) ENERCALC INC 1983-2021

Project File: 3.1 PGE GEN calcs.ec6

**DESCRIPTION:** Generator Reinforced Concrete Slab On Grade - Strength and Stability Analysis

#### **Code References**

Calculations per ACI 318-14, IBC 2018, CBC 2019, ASCE 7-16

Load Combinations Used: ASCE 7-16

#### **General Information**

Material Properties				Soil Design Values		
f'c : Concrete 28 day strength	=	2	.50 ksi	Allowable Soil Bearing	=	1.0 ksf
fy : Rebar Yield	=	6	0.0 ksi	Soil Density	=	110.0 pcf
Ec : Concrete Elastic Modulus	=	,	0.0 ksi	Increase Bearing By Footing Weight	=	No .
Concrete Density	=	15	0.0 pcf	Soil Passive Resistance (for Sliding)	=	100.0 pcf
<sub>0</sub> Values Flexure	=	0	.90	Soil/Concrete Friction Coeff.	=	0.30
' Shear	=	0.7	<b>'</b> 50	Increases based on footing Depth		
Analysis Settings				Footing base depth below soil surface	=	0.3330 ft
Min Steel % Bending Reinf.		=		Allow press. increase per foot of depth	=	ksf
Min Allow % Temp Reinf.		=	0.00180	when footing base is below	=	ft
Min. Overturning Safety Factor		=	1.0 : 1	Ç		
Min. Sliding Safety Factor		=	1.0 : 1	Increases based on footing plan dimension	on	
Add Ftg Wt for Soil Pressure		:	Yes	Allowable pressure increase per foot of de	epth	
Use ftg wt for stability, moments & shea	ırs	:	Yes		=	ksf
Add Pedestal Wt for Soil Pressure			No	when max. length or width is greater than		£.
Use Pedestal wt for stability, mom & sh	ear	:	No		=	ft

#### **Dimensions**

Width parallel to X-X Axis	=	9.160 ft
Length parallel to Z-Z Axis	=	15.0 ft
Footing Thickness	=	6.0 in
Load location offset from footing	g center	
ex : Prll to X-X Axis	=	6 in
ez : Prll to Z-Z Axis	=	6 in
Pedestal dimensions		
px : parallel to X-X Axis	=	35.0 in
pz : parallel to Z-Z Axis	=	116.0 in
Height	_	1.0 in
Rebar Centerline to Edge of Co	ncrete	
at Bottom of footing	=	3.0 in

# 2-11" 15'-0" Edge Dist. 5'-0-15/16" 9'-1-15/16"

#### Reinforcing

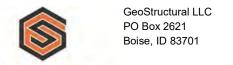
Bars parallel to X-X Axis Number of Bars Reinforcing Bar Size	= =	15.0 # 4
Bars parallel to Z-Z Axis Number of Bars Reinforcing Bar Size	= =	10.0 # 4
Bandwidth Distribution C Direction Requiring Closer	`	4.4.2)
seassquiinig Globol	•	ong X-X Axis

# Bars required within zone 75.8 % # Bars required on each side of zone 24.2 %

Z-Z Section Looking to +X X-X Section Looking to +Z

#### **Applied Loads**

		D	Lr	L	S	w	E	Н
P : Column Load	= _	6.683					-1.60	k
OB : Overburden	= _							ksf
M-xx	=					1.90	6.660	k-ft
M-zz	= _					5.80	6.660	k-ft
V-x	=					1.440	2.410	k
V-z	=					-0.470	-2.410	k



Project Title: Engineer: Project ID: AT&T Generator Upgrade Project Jesse Drennen, PE

ngineer: Jesse Drennen,

:

Project Descr: Standby Generator on Concrete Slab

# GEOSTRUCTURAL General Footing

LIC# : KW-06015027, Build:20.22.1.12

GeoStructural, LLC

Project File: 3.1 PGE GEN calcs.ec6
(c) ENERCALC INC 1983-2021

**DESCRIPTION:** Generator Reinforced Concrete Slab On Grade - Strength and Stability Analysis

DL	ESIGN SU	JMMARY				Design OK
		Min. Ratio	Item	Applied	Capacity	Governing Load Combination
	PASS	0.1739	Soil Bearing	0.1739 ksf	1.0 ksf	+D+0.70E
	PASS	6.033	Overturning - X-X	12.502 k-ft	75.425 k-ft	+0.60D+0.70E
	PASS	4.373	Overturning - Z-Z	10.216 k-ft	44.678 k-ft	+0.60D+0.70E
	PASS	1.663	Sliding - X-X	1.687 k	2.805 k	+0.60D+0.70E
	PASS	1.644	Sliding - Z-Z	1.687 k	2.773 k	+0.60D+0.70E
	PASS	9.101	Uplift	-1.120 k	10.193 k	+0.60D+0.70E
	PASS	0.3345	Z Flexure (+X)	0.8324 k-ft/ft	2.488 k-ft/ft	+1.440D+E
	PASS	0.5456	Z Flexure (-X)	1.358 k-ft/ft	2.488 k-ft/ft	+1.440D-E
	PASS	0.2112	X Flexure (+Z)	0.5692 k-ft/ft	2.695 k-ft/ft	+1.440D+E
	PASS	0.3879	X Flexure (-Z)	1.046 k-ft/ft	2.695 k-ft/ft	+1.440D-E
	PASS	0.210	1-way Shear (+X)	15.753 psi	75.0 psi	+1.440D+E
	PASS	0.2583	1-way Shear (-X)	19.369 psi	75.0 psi	+1.440D-E
	PASS	0.1746	1-way Shear (+Z)	13.096 psi	75.0 psi	+1.440D+E
	PASS	0.2086	1-way Shear (-Z)	15.645 psi	75.0 psi	+1.440D-E
	PASS	0.2386	2-way Punching	21.318 psi	89.331 psi	+1.440D-E

#### **Detailed Results**

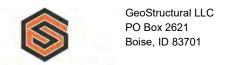
	Xecc	Zecc	Actual	Soil Bearing	Stress @ Loca	ation	Actual / Allow
Gross Allowable	(	in)	Bottom Left	Top Left	Top Right B	ottom Right	Ratio
							0.000
1.0	2.360	2.360	0.1175	0.09824	0.1298	0.1490	0.149
							0.000
1.0	5.175	3.049	0.1015	0.07662	0.1458	0.1707	0.171
							0.000
1.0	7.051	3.509	0.05451	0.03733	0.09386	0.1110	0.111
							0.000
1.0	6.373	4.885	0.09433	0.05710	0.1366	0.1739	0.174
							0.000
1.0	9.379	6.776	0.04733	0.01780	0.08473	0.1143	0.114
	1.0 1.0 1.0 1.0	Gross Allowable     (       1.0     2.360       1.0     5.175       1.0     7.051       1.0     6.373	Gross Allowable     (in)       1.0     2.360     2.360       1.0     5.175     3.049       1.0     7.051     3.509       1.0     6.373     4.885	Gross Allowable         (in)         Bottom Left           1.0         2.360         2.360         0.1175           1.0         5.175         3.049         0.1015           1.0         7.051         3.509         0.05451           1.0         6.373         4.885         0.09433	Gross Allowable         (in)         Bottom Left         Top Left           1.0         2.360         2.360         0.1175         0.09824           1.0         5.175         3.049         0.1015         0.07662           1.0         7.051         3.509         0.05451         0.03733           1.0         6.373         4.885         0.09433         0.05710	Gross Allowable         (in)         Bottom Left         Top Left         Top Right         B           1.0         2.360         2.360         0.1175         0.09824         0.1298           1.0         5.175         3.049         0.1015         0.07662         0.1458           1.0         7.051         3.509         0.05451         0.03733         0.09386           1.0         6.373         4.885         0.09433         0.05710         0.1366	Gross Allowable         (in)         Bottom Left         Top Left         Top Right         Bottom Right           1.0         2.360         2.360         0.1175         0.09824         0.1298         0.1490           1.0         5.175         3.049         0.1015         0.07662         0.1458         0.1707           1.0         7.051         3.509         0.05451         0.03733         0.09386         0.1110           1.0         6.373         4.885         0.09433         0.05710         0.1366         0.1739

#### **Overturning Stability**

Rotation Axis & Load Combination	Overturning Moment	Resisting Moment	Stability Ratio	Status
X-X, D Only	None	124.069 k-ft	Infinity	OK
X-X. +D+0.60W	1.140 k-ft	124.233 k-ft	108.976	OK
X-X, +0.60D+0.60W	1.140 k-ft	74.606 k-ft	65.444	OK
X-X, +D+0.70E	12.502 k-ft	125.053 k-ft	10.003	OK
X-X, +0.60D+0.70E	12.502 k-ft	75.425 k-ft	6.033	OK
Z-Z, D Only	None	74.464 k-ft	Infinity	OK
Z-Z, +D+0.60W	3.984 k-ft	74.464 k-ft	18.691	OK
Z-Z, +0.60D+0.60W	3.984 k-ft	44.678 k-ft	11.214	OK
Z-Z, +D+0.70E	10.216 k-ft	74.464 k-ft	7.289	OK
Z-Z, +0.60D+0.70E	10.216 k-ft	44.678 k-ft	4.373	OK
liding Stability				All units k

### **Sliding Stability**

Force Application Axis				
Load Combination	Sliding Force	Resisting Force	Stability Ratio	Status
X-X, D Only	0.0 k	5.180 k	No Sliding	OK
X-X, +D+0.60W	0.8640 k	5.180 k	5.995	OK
X-X, +0.60D+0.60W	0.8640 k	3.141 k	3.635	OK
X-X, +D+0.70E	1.687 k	4.844 k	2.871	OK
X-X, +0.60D+0.70E	1.687 k	2.805 k	1.663	OK
Z-Z, D Only	0.0 k	5.147 k	No Sliding	OK
Z-Z, +D+0.60W	-0.2820 k	5.147 k	18.252	OK
Z-Z, +0.60D+0.60W	-0.2820 k	3.109 k	11.024	OK
Z-Z, +D+0.70E	-1.687 k	4.811 k	2.852	OK
Z-Z, +0.60D+0.70E	-1.687 k	2.773 k	1.644	OK



Project Title: Engineer:

AT&T Generator Upgrade Project Jesse Drennen, PE

Project ID:

Project Descr: Standby Generator on Concrete Slab

## **General Footing**

LIC#: KW-06015027, Build:20.22.1.12

**GEOSTRUCTURAL** 

GeoStructural, LLC

Project File: 3.1 PGE GEN calcs.ec6

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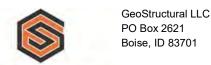
**DESCRIPTION:** Generator Reinforced Concrete Slab On Grade - Strength and Stability Analysis

#### **Footing Flexure**

Flexure Axis & Load Combination	n <mark>Mu</mark> k-ft	Side	Tension Surface	As Req'd in^2	Gvrn. As in^2	Actual As in^2	Phi*Mn k-ft	Status
X-X, +1.40D	0.4924	+Z	Bottom	0.1296	AsMin	0.2183	2.695	ОК
X-X, +1.40D	0.8552	-Z	Bottom	0.1296	AsMin	0.2183	2.695	oĸ
X-X, +1.20D+W	0.4896	+Z	Bottom	0.1296	AsMin	0.2183	2.695	ok
X-X, +1.20D+W	0.6095	-Z	Bottom	0.1296	AsMin	0.2183	2.695	oĸ
X-X, +1.20D-W	0.3847	+Z	Bottom	0.1296	AsMin	0.2183	2.695	oĸ
X-X, +1.20D-W	0.8566	-Z	Bottom	0.1296	AsMin	0.2183	2.695	ok
X-X, +0.90D+W	0.3841	+Z	Bottom	0.1296	AsMin	0.2183	2.695	oĸ
X-X, +0.90D+W	0.4262	-Z	Bottom	0.1296	AsMin	0.2183	2.695	OK
X-X, +0.90D-W	0.2999	+Z	Bottom	0.1296	AsMin	0.2183	2.695	OK
X-X, +0.90D-W	0.6733	-Z	Bottom	0.1296	AsMin	0.2183	2.695	OK
X-X, +1.440D+E	0.5692	+Z	Bottom	0.1296	AsMin	0.2183	2.695	OK
X-X, +1.440D+E	0.7138	-Z	Bottom	0.1296	AsMin	0.2183	2.695	OK
X-X, +1.440D-E	0.4676	+Z	Bottom	0.1296	AsMin	0.2183	2.695	OK
X-X, +1.440D-E	1.046	-Z	Bottom	0.1296	AsMin	0.2183	2.695	OK
X-X, +0.660D+E	0.2948	+Z	Bottom	0.1296	AsMin	0.2183	2.695	OK
X-X, +0.660D+E	0.2373	-Z	Bottom	0.1296	AsMin	0.2183	2.695	OK
X-X, +0.660D-E	0.2472	+Z	Bottom	0.1296	AsMin	0.2183	2.695	OK
X-X, +0.660D-E	0.5864	-Z	Bottom	0.1296	AsMin	0.2183	2.695	OK
Z-Z, +1.40D	1.137	-X	Bottom	0.1296	AsMin	0.20	2.488	OK
Z-Z. +1.40D	0.7190	+X	Bottom	0.1296	AsMin	0.20	2.488	OK
Z-Z, +1.20D+W	0.8396	-X	Bottom	0.1296	AsMin	0.20	2.488	OK
Z-Z, +1.20D+W	0.7204	+X	Bottom	0.1296	AsMin	0.20	2.488	OK
Z-Z, +1.20D-W	1.110	-X	Bottom	0.1296	AsMin	0.20	2.488	OK
Z-Z, +1.20D-W	0.5123	+X	Bottom	0.1296	AsMin	0.20	2.488	OK
Z-Z, +0.90D+W	0.5960	-X	Bottom	0.1296	AsMin	0.20	2.488	OK
Z-Z, +0.90D+W	0.5663	+X	Bottom	0.1296	AsMin	0.20	2.488	OK
Z-Z. +0.90D-W	0.8661	-X	Bottom	0.1296	AsMin	0.20	2.488	ok
Z-Z, +0.90D-W	0.3582	+X	Bottom	0.1296	AsMin	0.20	2.488	oĸ
Z-Z, +1.440D+E	0.9817	-X	Bottom	0.1296	AsMin	0.20	2.488	oĸ
Z-Z, +1.440D+E	0.8324	+X	Bottom	0.1296	AsMin	0.20	2.488	oĸ
Z-Z, +1.440D-E	1.358	-X	Bottom	0.1296	AsMin	0.20	2.488	oĸ
Z-Z, +1.440D-E	0.6467	+X	Bottom	0.1296	AsMin	0.20	2.488	oĸ
Z-Z, +0.660D+E	0.3482	-X	Bottom	0.1296	AsMin	0.20	2.488	ok
Z-Z, +0.660D+E	0.4318	+X	Bottom	0.1296	AsMin	0.20	2.488	OK
Z-Z, +0.660D-E	0.7601	-X	Bottom	0.1296	AsMin	0.20	2.488	OK
Z-Z, +0.660D-E	0.2702	+X	Bottom	0.1296	AsMin	0.20	2.488	OK
One Way Shear								
Load Combination	Vu @ -X	Vu @ -	+X Vu (	@ -Z Vu @	@ +Z \	/u:Max Phi Vn	Vu / Phi*Vn	Status
+1.40D	16.56	osi 1	13.74 psi	14.70 psi	11.35 psi	16.56 psi 7:	5.00 psi 0.22	OK

#### +1.40D 16.56 psi 13.74 psi 14.70 psi 11.35 psi 16.56 psi 75.00 psi 0.22 +1.20D+W 13.63 psi 14.22 psi 11.28 psi 14.22 psi 75.00 psi 0.19 OK 12.58 psi +1.20D-W 9.92 psi 12.05 psi 8.87 psi 15.80 psi 75.00 psi 0.21 15.80 psi OK 11.06 psi 8.85 psi 11.06 psi 75.00 psi +0.90D+W 9.04 psi 10.68 psi 0.15 OK +0.90D-W 6.98 psi 9.58 psi 6.92 psi 12.26 psi 75.00 psi 0.16 OK 12.26 psi +1.440D+E 14.70 psi 15.75 psi 15.41 psi 13.10 psi 15.75 psi 75.00 psi 0.21 OK +1.440D-E 19.37 psi 12.51 psi 15.65 psi 10.80 psi 19.37 psi 75.00 psi 0.26 OK 8.10 psi 8.10 psi 7.22 psi 6.77 psi +0.660D+E 75.00 psi 0.11 OK 5.47 psi +0.660D-E 5.31 psi 9.23 psi 5.72 psi 10.67 psi 75.00 psi 0.14 OK 10.67 psi Two-Way "Punching" Shear All units k

Load Combination	Vu	Phi*Vn	Vu / Phi*Vn	Status
+1.40D	19.31 psi	89.33 psi	0.2161	OK
+1.20D+W	16.42 psi	89.33 psi	0.1838	OK
+1.20D-W	16.67 psi	89.33 psi	0.1867	OK
+0.90D+W	12.28 psi	89.33 psi	0.1375	OK
+0.90D-W	12.54 psi	89.33 psi	0.1403	OK
+1.440D+E	18.40 psi	89.33 psi	0.2059	OK
+1.440D-E	21.32 psi	89.33 psi	0.2386	OK
+0.660D+E	7.64 psi	89.33 psi	0.08553	OK
+0.660D-E	10.56 psi	89.33 psi	0.1182	OK



Project Title: Engineer:

AT&T Generator Upgrade Project

Jesse Drennen, PE

Project ID: Project Descr:

Standby Generator on Concrete Slab



#### **Beam on Elastic Foundation**

Project File: 3.1 PGE GEN calcs.ec6

(c) ENERCALC INC 1983-2021

LIC#: KW-06015027, Build:20.22.1.12 GeoStructural, LLC **DESCRIPTION:** Slab On Grade - "Beam" on Soil Spring Design

**CODE REFERENCES** 

Calculations per ACI 318-14, IBC 2018, CBC 2019, ASCE 7-16

Load Combinations Used: ASCE 7-16

**Material Properties** 

2.50 ksi → Phi Values Flexure: 0.90  $fr = f'c^{1/2}$  7.50 375.0 psi Shear: 0.750 ₩ Density 150.0 pcf 0.850  $\beta_1$ 1.0

λ Lt Wt Factor Elastic Modulus 2,850.0 ksi

Soil Subgrade Modulus 47.0 psi / (inch deflection)

Load Combination ASCE 7-16

fy - Main Rebar Fy - Stirrups 40.0 ksi 60.0 ksi E - Main Rebar = 29,000.0 ksiE - Stirrups =29,000.0 ksiStirrup Bar Size # 3

> Number of Resisting Legs Per Stirrup 2

Beam is supported on an elastic foundation,



110" w x 6" h Span=15.0 ft

**Cross Section & Reinforcing Details** 

Rectangular Section, Width = 110.0 in, Height = 6.0 in Span #1 Reinforcing....

10-#4 at 3.0 in from Top, from 0.0 to 15.0 ft in this span

**Applied Loads** 

Service loads entered. Load Factors will be applied for calculations.

Design OK

Beam self weight calculated and added to loads

Load for Span Number 1

Moment: W = 1.90, E = 6.660 k-ft, Location = 6.50 ft from left end of this span

Point Load: D = 6.683 k @ 6.50 ft Point Load : E = 1.60 k @ 6.50 ft

DESIGN SUMMARY

**0.588**: 1 Maximum Deflection

Maximum Bending Stress Ratio = Max Downward L+Lr+S Deflection 0.000 in Section used for this span **Typical Section** Max Upward L+Lr+S Deflection 0.000 in Mu: Applied 14.508 k-ft Max Downward Total Deflection Mn \* Phi : Allowable 0.029 in 24.690 k-ft Max Upward Total Deflection 0.007 in +1.440D+E **Load Combination** 

Location of maximum on span 6.529 ft Span # where maximum occurs Span # 1

Maximum Soil Pressure = 0.198 ksf 7.17 ft LdComb: +D+0.70E at

Allowable Soil Pressure = **1.0** ksf OK

**Shear Stirrup Requirements** 

Entire Beam Span Length: Vu < PhiVc/2, Req'd Vs = Not Reqd, use stirrups spaced at 0.000 in

**Maximum Forces & Stresses for Load Combination** 

Load Co	ombination		Location (ft)	3ending	Stress Resu	ılts (k-ft
S	egment Length	Span #	in Span	Mu : Max	Phi*Mnx	Stress Ratio
MAXimu	ım Bending Enve	elope				
Span	n # 1	1	6.529	14.51	24.69	0.59
+1 40D						



GeoStructural LLC Project Title: Engineer: Project ID: PO Box 2621 Boise, ID 83701

AT&T Generator Upgrade Project Jesse Drennen, PE

Project Descr: Standby Generator on Concrete Slab



## **Beam on Elastic Foundation**

LIC#: KW-06015027, Build:20.22.1.12 GeoStructural, LLC Project File: 3.1 PGE GEN calcs.ec6 (c) ENERCALC INC 1983-2021

### **DESCRIPTION:** Slab On Grade - "Beam" on Soil Spring Design

Load Combination		Location (ft)	3ending	Stress Resu	ılts (k-ft
Segment Length	Span #	in Span	Mu : Max	Phi*Mnx	Stress Ratio
Span # 1	1	6.529	9.27	24.69	0.38
+1.20D+W					
Span # 1	1	6.529	8.91	24.69	0.36
+1.20D-W					
Span # 1	1	6.353	8.39	24.69	0.34
+0.90D+W					
Span # 1	1	6.529	6.93	24.69	0.28
+0.90D-W					
Span # 1	1	6.353	6.52	24.69	0.26
+1.440D+E					
Span # 1	1	6.529	14.51	24.69	0.59
+1.440D-E					
Span # 1	1	6.353	10.62	24.69	0.43
+0.660D+E					
Span # 1	1	6.529	9.34	24.69	0.38
+0.660D-E					
Span # 1	1	6.353	5.75	24.69	0.23

## **Overall Maximum Deflections - Unfactored Lo**

Load Combination	mbination Span Max. "-" Defl Locati		ation in Span	Load Combination	Max. "+" Defl Location in Span		
Span 1	1	0.0292	7.167		0.0000	0.000	

#### **Detailed Shear Information**

		Distance		Vu	(k)	Mu	d*Vu/Mu		Comment	Phi*Vs	Spacin	
Load Combination	Number	` '	(in)	Actual	Design	(k-ft)		(k)		(k)	Req'd S	
+0.660D-E	1	0.00	3.00	0.07		0.00			Vu < PhiVc/2	Not Reqd	0.00	0.00
+0.660D-E	1	0.18	3.00	0.09		0.00			Vu < PhiVc/2	Not Reqd	0.00	0.00
+0.660D-E	1	0.35	3.00	0.12		0.01			Vu < PhiVc/2	Not Reqd	0.00	0.00
+0.660D-E	1	0.53	3.00	0.14		0.02			Vu < PhiVc/2	Not Reqd	0.00	0.00
+0.660D-E	1	0.71	3.00	0.17		0.03			Vu < PhiVc/2	Not Reqd	0.00	0.00
+0.660D-E	1	0.88	3.00	0.21		0.05			Vu < PhiVc/2	Not Reqd	0.00	0.00
+1.440D-E	1	1.06	3.00	0.26		0.06			Vu < PhiVc/2	Not Reqd	0.00	0.00
+1.440D-E	1	1.24	3.00	0.32		0.10			Vu < PhiVc/2	Not Reqd	0.00	0.00
+1.440D-E	1	1.41	3.00	0.38		0.14			Vu < PhiVc/2	Not Reqd	0.00	0.00
+1.440D-E	1	1.59	3.00	0.46		0.20			Vu < PhiVc/2	Not Reqd	0.00	0.00
+1.440D-E	1	1.76	3.00	0.54		0.27			Vu < PhiVc/2	Not Reqd	0.00	0.00
+1.440D-E	1	1.94	3.00	0.63		0.35			Vu < PhiVc/2	Not Reqd	0.00	0.00
+1.440D-E	1	2.12	3.00	0.72		0.45			Vu < PhiVc/2	Not Reqd	0.00	0.00
+1.440D-E	1	2.29	3.00	0.83		0.57			Vu < PhiVc/2	Not Reqd	0.00	0.00
+1.440D-E	1	2.47	3.00	0.94		0.71			Vu < PhiVc/2	Not Reqd	0.00	0.00
+1.440D-E	1	2.65	3.00	1.06		0.86			Vu < PhiVc/2	Not Reqd	0.00	0.00
+1.440D-E	1	2.82	3.00	1.18		1.04			Vu < PhiVc/2	Not Reqd	0.00	0.00
+1.440D-E	1	3.00	3.00	1.31		1.23			Vu < PhiVc/2	Not Reqd	0.00	0.00
+1.440D-E	1	3.18	3.00	1.45		1.46			Vu < PhiVc/2	Not Reqd	0.00	0.00
+1.440D-E	1	3.35	3.00	1.60		1.70			Vu < PhiVc/2	Not Reqd	0.00	0.00
+1.440D-E	1 1	3.53	3.00	1.75		1.97			Vu < PhiVc/2	Not Reqd	0.00	0.00
+1.440D-E	1	3.71	3.00	1.91 2.08		2.27			Vu < PhiVc/2 Vu < PhiVc/2	Not Reqd	0.00	0.00
+1.440D-E	1	3.88 4.06		2.08		2.60 2.96			Vu < PhiVc/2	Not Reqd	0.00 0.00	0.00
+1.440D-E +1.440D-E	=	4.06	3.00			3.34			Vu < PhiVc/2	Not Reqd Not Regd		0.00
+1.440D-E +1.440D-E	1 1	4.24 4.41	3.00	2.43 2.61	2.43	3.76			Vu < PhiVc/2	Not Regd	0.00 0.00	0.00
+1.440D-E +1.440D-E	1	4.41	3.00	2.80		4.21			Vu < PhiVc/2	Not Regd	0.00	0.00
+1.440D-E +1.440D-E	1	4.76	3.00	2.00		4.69			Vu < PhiVc/2	Not Regd	0.00	0.00
+1.440D-E +1.440D-E	1	4.76	3.00	3.19		5.21			Vu < PhiVc/2	Not Regd	0.00	0.00
+1.440D-E +1.440D-E	1	5.12	3.00	3.19		5.76			Vu < PhiVc/2	Not Requ	0.00	0.00
+1.440D-E +1.440D-E	1	5.12	3.00	3.59		6.35	5 1.00		Vu < PhiVc/2	Not Regd	0.00	0.00
+1.440D-E +1.440D-E	1	5.47	3.00	3.79		6.97			Vu < PhiVc/2	Not Regd	0.00	0.00
+1.440D-E	1	5.65	3.00	4.00		7.63			Vu < PhiVc/2	Not Regd	0.00	0.00
+1.440D-E	1	5.82	3.00	4.20		8.32			Vu < PhiVc/2	Not Regd	0.00	0.00
+1.440D-E	i	6.00	3.00	4.41		9.05			Vu < PhiVc/2	Not Regd	0.00	0.00
+1.440D-E	1	6.18	3.00	4.61	4.61	9.82			Vu < PhiVc/2	Not Regd	0.00	0.00
+1.440D-E	1	6.35	3.00	4.81		10.62			Vu < PhiVc/2	Not Regd	0.00	0.00
+1.440D+E	i	6.53	3.00	-6.36		14.51			Vu < PhiVc/2	Not Regd	0.00	0.00
+1.440D+E	1	6.71	3.00	-6.08		13.37			Vu < PhiVc/2	Not Regd	0.00	0.00
+1.440D+E	i	6.88	3.00	-5.79		12.29			Vu < PhiVc/2	Not Regd	0.00	0.00
+1.440D+E	i 1	7.06	3.00	<b>-</b> 5.50		11.26			Vu < PhiVc/2	Not Regd	0.00	0.00
+1.440D+E	i	7.24	3.00	-5.22		10.28			Vu < PhiVc/2	Not Regd	0.00	0.00
+1.440D+E	i 1	7.41	3.00	-4.93		9.35			Vu < PhiVc/2	Not Regd	0.00	0.00
+1.440D+E	i	7.59	3.00	-4.65		8.46			Vu < PhiVc/2	Not Regd	0.00	0.00
	•		0.00	00		0.10		0			0.00	0.00



Project Title: AT&T Generator Upgrade Project Engineer: Jesse Drennen, PE Project ID: Project Descr: Standby Generator on Concrete Slab



## **Beam on Elastic Foundation**

GeoStructural, LLC

(c) ENERCALC INC 1983-2021

Project File: 3.1 PGE GEN calcs.ec6

**DESCRIPTION:** Slab On Grade - "Beam" on Soil Spring Design

### **Detailed Shear Information**

LIC#: KW-06015027, Build:20.22.1.12

Detailed Silear IIII												
		Distance		Vu	(k)	Mu	d*Vu/Mu		Comment	Phi*Vs	Spacin	
Load Combination	Number	(ft)	(in)	Actual	Design	(k-ft)		(k)		(k)	Req'd S	
+1.440D+E	1	7.76	3.00	-4.38		7.63		27.26	Vu < PhiVc/2	Not Reqd	0.00	0.00
+1.440D+E	1	7.94	3.00	<b>-</b> 4.10		6.85		27.26	Vu < PhiVc/2	Not Reqd	0.00	0.00
+1.440D+E	1	8.12	3.00	-3.84		6.11		27.26	Vu < PhiVc/2	Not Reqd	0.00	0.00
+1.440D+E	1	8.29	3.00	-3.57		5.43		27.26	Vu < PhiVc/2	Not Reqd	0.00	0.00
+1.440D+E	1	8.47	3.00	-3.32		4.79		27.26	Vu < PhiVc/2	Not Reqd	0.00	0.00
+1.440D+E	1	8.65	3.00	-3.07		4.19		27.26	Vu < PhiVc/2	Not Reqd	0.00	0.00
+1.440D+E	1	8.82	3.00	-2.83	2.83	3.64	1.00	27.26	Vu < PhiVc/2	Not Reqd	0.00	0.00
+1.440D+E	1	9.00	3.00	-2.60	2.60	3.13	1.00	27.26	Vu < PhiVc/2	Not Reqd	0.00	0.00
+1.440D+E	1	9.18	3.00	-2.37	2.37	2.66	1.00	27.26	Vu < PhiVc/2	Not Reqd	0.00	0.00
+1.440D+E	1	9.35	3.00	-2.15	2.15	2.23	1.00	27.26	Vu < PhiVc/2	Not Regd	0.00	0.00
+1.440D+E	1	9.53	3.00	-1.95	1.95	1.84	1.00	27.26	Vu < PhiVc/2	Not Reqd	0.00	0.00
+1.440D+E	1	9.71	3.00	-1.75	1.75	1.48	1.00	27.26	Vu < PhiVc/2	Not Reqd	0.00	0.00
+1.440D+E	1	9.88	3.00	-1.56	1.56	1.17	1.00	27.26	Vu < PhiVc/2	Not Regd	0.00	0.00
+1.440D+E	1	10.06	3.00	-1.37	1.37	0.88		27.26	Vu < PhiVc/2	Not Regd	0.00	0.00
+1.440D+E	1	10.24	3.00	-1.20	1.20	0.63	1.00	27.26	Vu < PhiVc/2	Not Regd	0.00	0.00
+1.440D+E	1	10.41	3.00	-1.04	1.04	0.40	1.00	27.26	Vu < PhiVc/2	Not Regd	0.00	0.00
+1.440D+E	1	10.59	3.00	-0.88	0.88	0.21	1.00	27.26	Vu < PhiVc/2	Not Regd	0.00	0.00
+1.440D+E	1	10.76	3.00	-0.74	0.74	0.04	1.00	27.26	Vu < PhiVc/2	Not Regd	0.00	0.00
+1.440D+E	1	10.94	3.00	-0.60	0.60	0.10	1.00	27.26	Vu < PhiVc/2	Not Regd	0.00	0.00
+1.440D+E	1	11.12	3.00	-0.48	0.48	0.22		27.26	Vu < PhiVc/2	Not Redd	0.00	0.00
+1.440D+E	1	11.29	3.00	-0.36		0.31		27.26	Vu < PhiVc/2	Not Regd	0.00	0.00
+0.660D-E	1	11.47	3.00	0.30	0.30	0.53		27.26	Vu < PhiVc/2	Not Reqd	0.00	0.00
+1.440D-E	1	11.65	3.00	0.30		0.84		27.26	Vu < PhiVc/2	Not Redd	0.00	0.00
+1.440D-E	1	11.82	3.00	0.33	0.33	0.79	1.00	27.26	Vu < PhiVc/2	Not Regd	0.00	0.00
+1.440D-E	1	12.00	3.00	0.35		0.75		27.26	Vu < PhiVc/2	Not Regd	0.00	0.00
+1.440D-E	1	12.18	3.00	0.37		0.70		27.26	Vu < PhiVc/2	Not Regd	0.00	0.00
+1.440D-E	1	12.35	3.00	0.38		0.64		27.26	Vu < PhiVc/2	Not Regd	0.00	0.00
+1.440D-E	1	12.53	3.00	0.39		0.58		27.26	Vu < PhiVc/2	Not Regd	0.00	0.00
+1.440D-E	1	12.71	3.00	0.39		0.53		27.26	Vu < PhiVc/2	Not Regd	0.00	0.00
+1.440D-E	1	12.88	3.00	0.39		0.47		27.26	Vu < PhiVc/2	Not Redd	0.00	0.00
+1.440D-E	1	13.06	3.00	0.39		0.41		27.26	Vu < PhiVc/2	Not Regd	0.00	0.00
+1.440D-E	1	13.24	3.00	0.38		0.35		27.26	Vu < PhiVc/2	Not Regd	0.00	0.00
+1.440D-E	1	13.41	3.00	0.36		0.29		27.26	Vu < PhiVc/2	Not Regd	0.00	0.00
+1.440D-E	1	13.59	3.00	0.34		0.24		27.26	Vu < PhiVc/2	Not Regd	0.00	0.00
+1.440D+E	1	13.76	3.00	0.32		0.21		27.26	Vu < PhiVc/2	Not Regd	0.00	0.00
+1.440D+E	1	13.94	3.00	0.31		0.16		27.26	Vu < PhiVc/2	Not Regd	0.00	0.00
+1.440D+E	i 1	14.12	3.00	0.28		0.12		27.26	Vu < PhiVc/2	Not Regd	0.00	0.00
+1.440D+E	i	14.29	3.00	0.25		0.08		27.26	Vu < PhiVc/2	Not Regd	0.00	0.00
+1.440D+E	1	14.47	3.00	0.21		0.05		27.26	Vu < PhiVc/2	Not Regd	0.00	0.00
+1.440D+E	1	14.65	3.00	0.15		0.02		27.26	Vu < PhiVc/2	Not Regd	0.00	0.00
+1.440D+E	1	14.82	3.00	0.13		0.02		27.26	Vu < PhiVc/2	Not Regd	0.00	0.00
· 1+0D · L	'	17.02	5.00	0.03	0.03	0.01	1.00	21.20	να ¬ Ι ΙΙΙν Ο/ Ζ	Not requ	0.00	0.00



#### www.hilti.com

 Company:
 GeoStructural, LLC
 Page:
 1

 Address:
 PO Box 2621
 Specifier:

 Phone I Fax:
 5305394787 |
 E-Mail:
 contact@geostructural.com

 Design:
 10088152 3
 Date:
 2/15/2022

 Fastening point:
 2/15/2022

Specifier's comments: Wet

## 1 Input data

Anchor type and diameter: Kwik Bolt TZ2 - SS 304 5/8 (3 1/4) hnom2

Item number: 2210278 KB-TZ2 5/8x4 3/4 SS304 Effective embedment depth:  $h_{ef.act} = 3.250$  in.,  $h_{nom} = 3.750$  in.

Material: AISI 304
Evaluation Service Report: ESR-4266

Issued I Valid: 7/1/2021 | 12/1/2021

Proof: Design Method ACI 318-14 / Mech

Stand-off installation:  $e_b = 0.000$  in. (no stand-off); t = 0.250 in.

Anchor plate<sup>R</sup>:  $I_x \times I_y \times t = 116.000$  in. x 36.000 in. x 0.250 in.; (Recommended plate thickness: not calculated)

Profile: no profile

Base material: cracked concrete, 2500,  $f_c$ ' = 2,500 psi; h = 6.000 in. Installation: hammer drilled hole, Installation condition: Dry

Reinforcement: tension: condition B, shear: condition B; no supplemental splitting reinforcement present

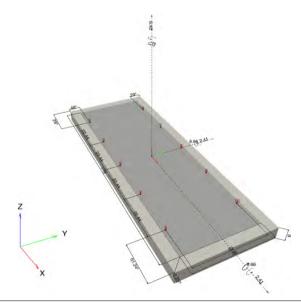
edge reinforcement: none or < No. 4 bar

Seismic loads (cat. C, D, E, or F)

Tension load: yes (17.2.3.4.3 (d))

Shear load: yes (17.2.3.5.3 (c))

#### Geometry [in.] & Loading [kip, ft.kip]







Input data and results must be checked for conformity with the existing conditions and for plausibility!
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<sup>&</sup>lt;sup>R</sup> - The anchor calculation is based on a rigid anchor plate assumption.





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#### 1.1 Unfactored loads

	Sustained	Load factor						
	load factor	f <sub>1</sub> or f <sub>2</sub>	V <sub>x</sub> [kip]	V <sub>y</sub> [kip]	N [kip]	M <sub>x</sub> [ft.kip]	M <sub>y</sub> [ft.kip]	M <sub>z</sub> [ft.kip]
D (Dead)	1.000	-	-	-	-6.683	-	-	-
F (Fluid)	1.000	-	-	-	-	-	-	-
T (Temperature)	1.000	-	-	-	-	-	-	-
L (Live)	1.000	0.500	-	-	-	-	-	-
H (Lateral)	1.000	-	-	-	-	-	-	-
L <sub>r</sub> (Roof live)	1.000	-	-	-	-	-	-	-
S (Snow)	1.000	0.200	-	-	-	-	-	-
R (Rain)	-	-	-	-	-	-	-	-
W (Wind)	-	-	0.470	1.440	-	-5.80000	1.90000	-
E (Earthquake)	-	-	2.410	2.410	1.600	-6.66000	6.66000	-

#### 1.2 Load combination and design results

#### 1.2.1 Load combination

Load case	Load combination
Equation (16-4a)	$1.2 (D + F) + 1.0 (W) + f_1L + 1.6 (H) + 0.5 (L_r)$
Equation (16-5)	1.2 (D + F) + 1.0 (E) + $f_1$ L + 1.6 (H) + $f_2$ S
Equation (16-6)	0.9 (D) + 1.0 (W) + 1.6 (H)
Equation (16-7)	0.9 (D + F) + 1.0 (E) + 1.6 (H)

#### 1.2.2 Design results

	Case	Description	Forces [kip] / Moments [ft.kip]	Seismic	Max. Util. Anchor [%]
-	Equation (16-4a)	1.2 (D + F) + 1.0 (W) + f <sub>1</sub> L + 1.6 (H) + 0.5 (L <sub>r</sub> )	$N = -8.020; V_x = 0.470; V_y = 1.440;$ $M_x = -5.80000; M_y = 1.90000; M_z = 0.00000;$	yes	9
	Equation (16-5)	1.2 (D + F) + 1.0 (E) + f <sub>1</sub> L + 1.6 (H) + f <sub>2</sub> S	$\frac{N = -6.420; \ V_{x} = 2.410; \ V_{y} = 2.410;}{M_{x} = -6.66000; \ M_{y} = 6.66000; \ M_{z} = 0.00000;}$	<u>yes</u>	<u>20</u>
	Equation (16-6)	0.9 (D) + 1.0 (W) + 1.6 (H)	$N = -6.015; V_x = 0.470; V_y = 1.440;$ $M_x = -5.80000; M_y = 1.90000; M_z = 0.00000;$	yes	9
	Equation (16-7)	0.9 (D + F) + 1.0 (E) + 1.6 (H)	$N = -4.415$ ; $V_x = 2.410$ ; $V_y = 2.410$ ; $M_x = -6.66000$ ; $M_y = 6.66000$ ; $M_z = 0.00000$ ;	yes	20





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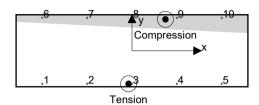
## 2 Load case/Resulting anchor forces

Controlling load case: Equation (16-5) 1.2 (D + F) + 1.0 (E) +  $f_1L$  + 1.6 (H) +  $f_2S$ 

#### Anchor reactions [kip]

Tension force: (+Tension, -Compression)

Anchor	Tension force	Shear force	Shear force x	Shear force y
1	0.070	0.341	0.241	0.241
2	0.068	0.341	0.241	0.241
3	0.065	0.341	0.241	0.241
4	0.063	0.341	0.241	0.241
5	0.060	0.341	0.241	0.241
6	0.000	0.341	0.241	0.241
7	0.000	0.341	0.241	0.241
8	0.000	0.341	0.241	0.241
9	0.000	0.341	0.241	0.241
10	0.000	0.341	0.241	0.241



 $\begin{array}{lll} \text{max. concrete compressive strain:} & 0.00 \ [\%] \\ \text{max. concrete compressive stress:} & 0.018 \ [\text{ksi}] \\ \text{resulting tension force in (x/y)=(-1.708/-16.508):} & 0.326 \ [\text{kip}] \\ \text{resulting compression force in (x/y)=(16.742/15.719):} & 4.741 \ [\text{kip}] \end{array}$ 

Anchor forces are calculated based on the assumption of a rigid anchor plate.

#### 3 Tension load

	Load N <sub>ua</sub> [kip]	Capacity P N <sub>n</sub> [kip] l	Jtilization $\beta_N = N_{ua}/\Phi N_n$	Status	
Steel Strength*	0.070	14.132	1	OK	
Pullout Strength*	N/A	N/A	N/A	N/A	
Concrete Breakout Failure**	0.326	11.104	3	OK	

<sup>\*</sup> highest loaded anchor \*\*anchor group (anchors in tension)





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#### 3.1 Steel Strength

 $\begin{array}{ll} N_{sa} & = \text{ESR value} & \text{refer to ICC-ES ESR-4266} \\ \phi \ N_{sa} \geq N_{ua} & \text{ACI 318-14 Table 17.3.1.1} \end{array}$ 

#### Variables

A<sub>se,N</sub> [in.<sup>2</sup>] f<sub>uta</sub> [ksi] 0.16 114.604

#### Calculations

N<sub>sa</sub> [kip] 18.843

N <sub>sa</sub> [kip]	$\phi_{steel}$	$\phi_{nonductile}$	φ N <sub>sa</sub> [kip]	N <sub>ua</sub> [kip]	
18 843	0.750	1 000	14 132	0.070	





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#### 3.2 Concrete Breakout Failure

 $=\left(\frac{A_{Nc}}{A_{Nc}}\right)_{NC}$ 

$N_{cbg} = \left(\frac{A_{Nc}}{A_{Nc0}}\right) \psi_{ec,N} \psi_{ed,N} \psi_{c,N} \psi_{cp,N} N_b$	ACI 318-14 Eq. (17.4.2.1b)
$\phi N_{cbg} \ge N_{ua}$	ACI 318-14 Table 17.3.1.1
A <sub>Nc</sub> see ACI 318-14, Section 17.4.2.1, Fig. R 17.4.2.1(b)	
$A_{Nc0} = 9 h_{ef}^2$	ACI 318-14 Eq. (17.4.2.1c)
$ \psi_{\text{ec,N}} = \left(\frac{1}{1 + \frac{2 e_{\text{N}}}{3 h_{\text{ef}}}}\right) \le 1.0 $	ACI 318-14 Eq. (17.4.2.4)
$\psi_{\text{ed,N}} = 0.7 + 0.3 \left( \frac{c_{a,\text{min}}}{1.5h_{\text{ef}}} \right) \le 1.0$	ACI 318-14 Eq. (17.4.2.5b)
$\psi_{cp,N} = MAX \left( \frac{c_{a,min}}{c_{ac}}, \frac{1.5h_{ef}}{c_{ac}} \right) \le 1.0$	ACI 318-14 Eq. (17.4.2.7b)
$N_{b} = k_{c} \lambda_{a} \sqrt{f_{c}^{c}} h_{ef}^{1.5}$	ACI 318-14 Eq. (17.4.2.2a)

#### **Variables**

h <sub>ef</sub> [in.]	e <sub>c1,N</sub> [in.]	e <sub>c2,N</sub> [in.]	c <sub>a,min</sub> [in.]	$\psi_{c,N}$
3.250	1.708	0.000	29.000	1.000
c <sub>ac</sub> [in.]	k <sub>c</sub>	λ <sub>a</sub>	f <sub>c</sub> [psi]	
7.000	21	1.000	2,500	

#### Calculations

A <sub>Nc</sub> [in. <sup>2</sup> ]	A <sub>Nc0</sub> [in. <sup>2</sup> ]	$\psi_{\text{ ec1,N}}$	$\psi_{\text{ec2,N}}$	$\psi_{\text{ed},N}$	$\psi_{\text{cp},N}$	N <sub>b</sub> [kip]
475.31	95.06	0.741	1.000	1.000	1.000	6.152

N <sub>cbg</sub> [kip]	φ <sub>concrete</sub>	$\phi_{\sf seismic}$	$\phi_{nonductile}$	φ N <sub>cbg</sub> [kip]	N <sub>ua</sub> [kip]
22.778	0.650	0.750	1.000	11.104	0.326





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### 4 Shear load

	Load V <sub>ua</sub> [kip]	Capacity <b>V</b> <sub>n</sub> [kip]	Utilization $\beta_V = V_{ua}/\Phi V_n$	Status
Steel Strength*	0.341	8.034	5	OK
Steel failure (with lever arm)*	N/A	N/A	N/A	N/A
Pryout Strength**	3.408	86.100	4	OK
Concrete edge failure in direction x+**	3.408	17.406	20	OK

### 4.1 Steel Strength

 $\begin{array}{lll} {\rm V_{sa,eq}} & = {\rm ESR~value} & {\rm refer~to~ICC\text{-}ES~ESR\text{-}4266} \\ {\rm \phi~V_{steel}} \geq {\rm V_{ua}} & {\rm ACI~318\text{-}14~Table~17.3.1.1} \end{array}$ 

#### **Variables**

$A_{se,V}$ [in. <sup>2</sup> ]	f <sub>uta</sub> [ksi]	$\alpha_{V,seis}$
0.16	114.604	1.000

#### Calculations

V<sub>sa,eq</sub> [kip] 12.360

V <sub>sa,eq</sub> [kip]	$\phi_{\text{steel}}$	$\phi_{nonductile}$	φ V <sub>sa,eq</sub> [kip]	V <sub>ua</sub> [kip]
12.360	0.650	1.000	8.034	0.341





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#### 4.2 Pryout Strength

$V_{cpg} = k_{cp} \left[ \left( \frac{A_{Nc}}{A_{Nc0}} \right) \psi_{ec,N} \psi_{ed,N} \psi_{c,N} \psi_{cp,N} N_b \right]$	ACI 318-14 Eq. (17.5.3.1b)
$\phi V_{cpg} \ge V_{ua}$	ACI 318-14 Table 17.3.1.1
A <sub>Nc</sub> see ACI 318-14, Section 17.4.2.1, Fig. R 17.4.2.1(b)	
$A_{Nc0} = 9 h_{ef}^2$	ACI 318-14 Eq. (17.4.2.1c)
$ \psi_{\text{ec,N}} = \left(\frac{1}{1 + \frac{2 e_{\text{N}}}{3 h_{\text{ef}}}}\right) \le 1.0 $	ACI 318-14 Eq. (17.4.2.4)
$\psi_{\text{ed,N}} = 0.7 + 0.3 \left( \frac{c_{a,\text{min}}}{1.5h_{\text{ef}}} \right) \le 1.0$	ACI 318-14 Eq. (17.4.2.5b)
$\psi_{\text{cp,N}} = \text{MAX} \left( \frac{c_{a,\text{min}}}{c_{ac}}, \frac{1.5h_{ef}}{c_{ac}} \right) \le 1.0$	ACI 318-14 Eq. (17.4.2.7b)
$N_b = k_c \lambda_a \sqrt{f_c} h_{ef}^{1.5}$	ACI 318-14 Eq. (17.4.2.2a)

#### Variables

k <sub>cp</sub>	h <sub>ef</sub> [in.]	e <sub>c1,N</sub> [in.]	e <sub>c2,N</sub> [in.]	c <sub>a,min</sub> [in.]
2	3.250	0.001	0.001	29.000
$\Psi_{c,N}$	c <sub>ac</sub> [in.]	k <sub>c</sub>	$\lambda$ a	f <sub>c</sub> [psi]
1.000	7.000	21	1.000	2,500

#### Calculations

A <sub>Nc</sub> [in. <sup>2</sup> ]	A <sub>Nc0</sub> [in. <sup>2</sup> ]	$\Psi_{\text{ec1,N}}$	$\Psi_{\text{ec2,N}}$	$\psi_{\text{ed},N}$	$\Psi_{cp,N}$	N <sub>b</sub> [kip]
950.63	95.06	1.000	1.000	1.000	1.000	6.152
Results						

V <sub>cpg</sub> [kip]	φ concrete	$\phi_{\sf seismic}$	$\phi_{nonductile}$	φ V <sub>cpg</sub> [kip]	V <sub>ua</sub> [kip]
122 999	0.700	1 000	1 000	86 100	3 408





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#### 4.3 Concrete edge failure in direction x+

$V_{cbg} = \left(\frac{A_{Vc}}{A_{Vc0}}\right) \psi_{ec,V} \psi_{ed,V} \psi_{c,V} \psi_{h,V} \psi_{parallel,V} V_{b}$	ACI 318-14 Eq. (17.5.2.1b)
$\phi V_{cbg} \ge V_{ua}$	ACI 318-14 Table 17.3.1.1
$A_{Vc}$ see ACI 318-14, Section 17.5.2.1, Fig. R 17.5.2.1(b) $A_{Vc0}$ = 4.5 $c_{a1}^2$	ACI 318-14 Eq. (17.5.2.1c)
$ \psi_{\text{ec,V}} = \left(\frac{1}{1 + \frac{2e_{v}}{3c_{a1}}}\right) \le 1.0 $	ACI 318-14 Eq. (17.5.2.5)
$\psi_{\text{ed,V}} = 0.7 + 0.3 \left( \frac{c_{a2}}{1.5c_{a1}} \right) \le 1.0$	ACI 318-14 Eq. (17.5.2.6b)
$\psi_{h,V} = \sqrt{\frac{1.5c_{a1}}{h_a}} \ge 1.0$	ACI 318-14 Eq. (17.5.2.8)
$V_{b} = \left(7 \left(\frac{I_{e}}{d_{a}}\right)^{0.2} \sqrt{d_{a}}\right) \lambda_{a} \sqrt{f_{c}} c_{a1}^{1.5}$	ACI 318-14 Eq. (17.5.2.2a)

#### Variables

c <sub>a1</sub> [in.]	c <sub>a2</sub> [in.]	e <sub>cV</sub> [in.]	$\Psi_{c,V}$	h <sub>a</sub> [in.]
32.000	29.000	0.000	1.000	6.000
l <sub>e</sub> [in.]	$\lambda$ a	d <sub>a</sub> [in.]	f <sub>c</sub> [psi]	$\psi$ parallel,V
3.250	1.000	0.625	2,500	1.000

#### Calculations

A <sub>Vc</sub> [in. <sup>2</sup> ]	A <sub>Vc0</sub> [in. <sup>2</sup> ]	$\psi_{\text{ec,V}}$	$\psi_{\text{ed,V}}$	$\psi_{h,V}$	V <sub>b</sub> [kip]
660.00	4,608.00	1.000	0.881	2.828	69.652

#### Results

V <sub>cbg</sub> [kip]	φ concrete	$\phi_{\sf seismic}$	$\phi_{nonductile}$	φ V <sub>cbg</sub> [kip]	V <sub>ua</sub> [kip]
24.866	0.700	1.000	1.000	17.406	3.408

## 5 Combined tension and shear loads

$\beta_{N}$	$\beta_{V}$	ζ	Utilization β <sub>N,V</sub> [%]	Status	
0.029	0.196	5/3	7	OK	

$$\beta_{NV} = \beta_N^{\zeta} + \beta_V^{\zeta} \le 1$$





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#### 6 Warnings

- The anchor design methods in PROFIS Engineering require rigid anchor plates per current regulations (AS 5216:2021, ETAG 001/Annex C, EOTA TR029 etc.). This means load re-distribution on the anchors due to elastic deformations of the anchor plate are not considered the anchor plate is assumed to be sufficiently stiff, in order not to be deformed when subjected to the design loading. PROFIS Engineering calculates the minimum required anchor plate thickness with CBFEM to limit the stress of the anchor plate based on the assumptions explained above. The proof if the rigid anchor plate assumption is valid is not carried out by PROFIS Engineering. Input data and results must be checked for agreement with the existing conditions and for plausibility!
- Condition A applies where the potential concrete failure surfaces are crossed by supplementary reinforcement proportioned to tie the potential concrete failure prism into the structural member. Condition B applies where such supplementary reinforcement is not provided, or where pullout or pryout strength governs.
- · Refer to the manufacturer's product literature for cleaning and installation instructions.
- For additional information about ACI 318 strength design provisions, please go to https://submittals.us.hilti.com/PROFISAnchorDesignGuide/
- An anchor design approach for structures assigned to Seismic Design Category C, D, E or F is given in ACI 318-14, Chapter 17, Section 17.2.3.4.3 (a) that requires the governing design strength of an anchor or group of anchors be limited by ductile steel failure. If this is NOT the case, the connection design (tension) shall satisfy the provisions of Section 17.2.3.4.3 (b), Section 17.2.3.4.3 (c), or Section 17.2.3.4.3 (d). The connection design (shear) shall satisfy the provisions of Section 17.2.3.5.3 (a), Section 17.2.3.5.3 (b), or Section 17.2.3.5.3 (c).
- Section 17.2.3.4.3 (b) / Section 17.2.3.5.3 (a) require the attachment the anchors are connecting to the structure be designed to undergo ductile yielding at a load level corresponding to anchor forces no greater than the controlling design strength. Section 17.2.3.4.3 (c) / Section 17.2.3.5.3 (b) waive the ductility requirements and require the anchors to be designed for the maximum tension / shear that can be transmitted to the anchors by a non-yielding attachment. Section 17.2.3.4.3 (d) / Section 17.2.3.5.3 (c) waive the ductility requirements and require the design strength of the anchors to equal or exceed the maximum tension / shear obtained from design load combinations that include E, with E increased by ω<sub>0</sub>.
- Hilti post-installed anchors shall be installed in accordance with the Hilti Manufacturer's Printed Installation Instructions (MPII). Reference ACI 318-14, Section 17.8.1.

## Fastening meets the design criteria!



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#### 7 Installation data

Profile: no profile

Hole diameter in the fixture:  $d_f = 0.687$  in.

Plate thickness (input): 0.250 in.

Recommended plate thickness: not calculated

Drilling method: Hammer drilled

Cleaning: Manual cleaning of the drilled hole according to instructions for use is

required.

Anchor type and diameter: Kwik Bolt TZ2 - SS 304 5/8 (3

1/4) hnom2

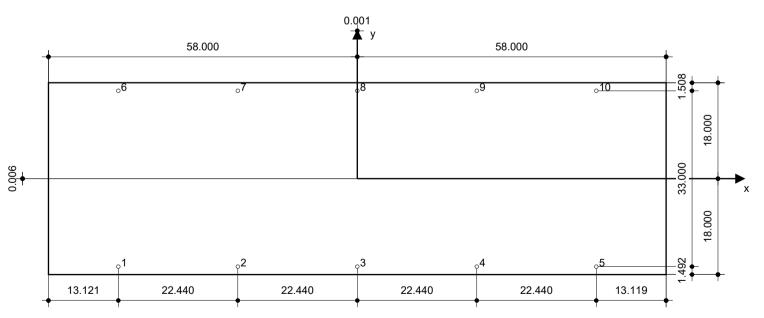
Item number: 2210278 KB-TZ2 5/8x4 3/4 SS304 Maximum installation torque: 0.06019 ft.kip Hole diameter in the base material: 0.625 in. Hole depth in the base material: 4.250 in.

Minimum thickness of the base material: 5.500 in.

Hilti KB-TZ2 stud anchor with 3.75 in embedment, 5/8 (3 1/4) hnom2, Stainless steel, installation per ESR-4266

#### 7.1 Recommended accessories

Drilling	Cleaning	Setting
Suitable Rotary Hammer	Manual blow-out pump	Torque controlled cordless impact tool
<ul> <li>Properly sized drill bit</li> </ul>		Torque wrench
		Hammer



#### Coordinates Anchor [in.]

Anchor	x	у	C <sub>-x</sub>	C+x	C <sub>-y</sub>	c <sub>+y</sub>	Anchor	x	у	C <sub>-x</sub>	C+x	c <sub>-y</sub>	C <sub>+y</sub>
1	-44.879	-16.508	29.000	151.000	48.000	62.000	6	-44.879	16.492	29.000	151.000	81.000	29.000
2	-22.439	-16.508	51.440	128.560	48.000	62.000	7	-22.439	16.492	51.440	128.560	81.000	29.000
3	0.001	-16.508	73.880	106.120	48.000	62.000	8	0.001	16.492	73.880	106.120	81.000	29.000
4	22.441	-16.508	96.320	83.680	48.000	62.000	9	22.441	16.492	96.320	83.680	81.000	29.000
5	44.881	-16.508	118.760	61.240	48.000	62.000	10	44.881	16.492	118.760	61.240	81.000	29.000

Input data and results must be checked for conformity with the existing conditions and for plausibility! PROFIS Engineering ( c ) 2003-2022 Hilti AG, FL-9494 Schaan Hilti is a registered Trademark of Hilti AG, Schaan





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#### 8 Remarks; Your Cooperation Duties

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- You must take all necessary and reasonable steps to prevent or limit damage caused by the Software. In particular, you must arrange for the
  regular backup of programs and data and, if applicable, carry out the updates of the Software offered by Hilti on a regular basis. If you do not use
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#### Specifier's comments:

## 1 Input data

Anchor type and diameter: Kwik Bolt TZ2 - SS 304 5/8 (3 1/4) hnom2

Item number:2210279 KB-TZ2 5/8x6 SS304Effective embedment depth: $h_{ef.act} = 3.250 \text{ in., } h_{nom} = 3.750 \text{ in.}$ 

Material: AISI 304
Evaluation Service Report: ESR-4266

Issued I Valid: 7/1/2021 | 12/1/2021

Proof: Design Method ACI 318-14 / Mech

Stand-off installation:  $e_b = 0.000$  in. (no stand-off); t = 0.500 in.

Anchor plate<sup>R</sup>:  $I_x \times I_y \times t = 3.000 \text{ in. } \times 0.500 \text{ in.; (Recommended plate thickness: not calculated)}$ 

Profile: no profile

Base material: cracked concrete, 2500,  $f_c$ ' = 2,500 psi; h = 6.000 in. Installation: hammer drilled hole, Installation condition: Dry

Reinforcement: tension: condition B, shear: condition B; no supplemental splitting reinforcement present

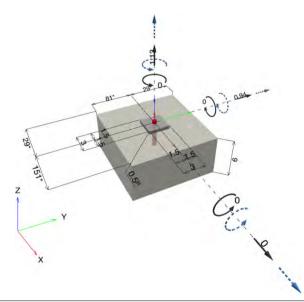
edge reinforcement: none or < No. 4 bar

Seismic loads (cat. C, D, E, or F)

Tension load: yes (17.2.3.4.3 (d))

Shear load: yes (17.2.3.5.3 (c))

#### Geometry [in.] & Loading [kip, ft.kip]







<sup>&</sup>lt;sup>R</sup> - The anchor calculation is based on a rigid anchor plate assumption.





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#### 1.1 Unfactored loads

	Sustained load factor	Load factor f <sub>1</sub> or f <sub>2</sub>	V <sub>x</sub> [kip]	V <sub>v</sub> [kip]	N [kip]	M <sub>x</sub> [ft.kip]	M <sub>v</sub> [ft.kip]	M <sub>z</sub> [ft.kip]
D (Dead)	1.000	_	-		_	-		
F (Fluid)	1.000	-	-	-	-	-	-	-
T (Temperature)	1.000	-	-	-	-	-	-	-
` L (Live)	1.000	0.500	-	-	-	-	-	-
H (Lateral)	1.000	-	-	-	-	-	-	-
L <sub>r</sub> (Roof live)	1.000	-	-	-	-	-	-	-
S (Snow)	1.000	0.200	-	-	-	-	-	-
R (Rain)	-	-	-	-	-	-	-	-
W (Wind)	-	-	-	-	-	-	-	-
E (Earthquake)	-	-	-	0.940	1.130	-	-	-

#### 1.2 Load combination and design results

#### 1.2.1 Load combination

	ise	Load combination
Equation (	16-7)	0.9 (D + F) + 1.0 (E) + 1.6 (H)

#### 1.2.2 Design results

Case	Description	Forces [kip] / Moments [ft.kip]	Seismic	Max. Util. Anchor [%]
Equation (16-7)	0.9 (D + F) + 1.0 (E) + 1.6 (H)	$N = 1.130$ ; $V_x = 0.000$ ; $V_y = 0.940$ ;	yes	38
		$M_{v} = 0.00000$ ; $M_{v} = 0.00000$ ; $M_{z} = 0.00000$ ;		

<sup>\*</sup> The detailed results (0.9 (D + F) + 1.0 (E) + 1.6 (H), shown in the following) do not represent the decisive load combination #DECISIVE#

## 2 Load case/Resulting anchor forces

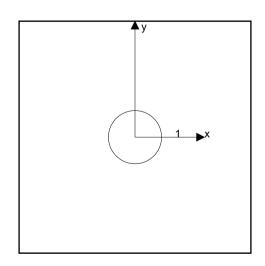
#### Anchor reactions [kip]

Tension force: (+Tension, -Compression)

Anchor	Tension force	Shear force	Shear force x	Shear force y
1	1.130	0.940	0.000	0.940

max. concrete compressive strain: - [%] max. concrete compressive stress: - [ksi] resulting tension force in (x/y)=(0.000/0.000): 1.130 [kip] resulting compression force in (x/y)=(0.000/0.000): 0.000 [kip]

Anchor forces are calculated based on the assumption of a rigid anchor plate.







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### 3 Tension load

	Load N <sub>ua</sub> [kip]	Capacity <b>P</b> N <sub>n</sub> [kip]	Utilization $\beta_N = N_{ua}/\Phi N_n$	Status
Steel Strength*	1.130	14.132	8	OK
Pullout Strength*	N/A	N/A	N/A	N/A
Concrete Breakout Failure**	1.130	2.999	38	OK

<sup>\*</sup> highest loaded anchor \*\*anchor group (anchors in tension)

#### 3.1 Steel Strength

 $\begin{array}{ll} {\rm N_{sa}} & = {\rm ESR} \ {\rm value} & {\rm refer} \ {\rm to} \ {\rm ICC\text{-}ES} \ {\rm ESR\text{-}4266} \\ \phi \ {\rm N_{sa}} \ge {\rm N_{ua}} & {\rm ACI} \ {\rm 318\text{-}14} \ {\rm Table} \ {\rm 17.3.1.1} \end{array}$ 

#### Variables

A<sub>se,N</sub> [in.<sup>2</sup>] f<sub>uta</sub> [ksi] 0.16 114.604

#### Calculations

N<sub>sa</sub> [kip] 18.843

N <sub>sa</sub> [kip]	φ <sub>steel</sub>	$\phi_{nonductile}$	φ N <sub>sa</sub> [kip]	N <sub>ua</sub> [kip]
18 843	0.750	1 000	14 132	1 130





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#### 3.2 Concrete Breakout Failure

$N_{cb} = \begin{pmatrix} \frac{A_{Nc}}{A_{Nc0}} \end{pmatrix} \psi_{ed,N} \psi_{c,N} \psi_{cp,N} N_b$	ACI 318-14 Eq. (17.4.2.1a)
$\phi N_{cb} \ge N_{ua}$	ACI 318-14 Table 17.3.1.1
A <sub>Nc</sub> see ACI 318-14, Section 17.4.2.1, Fig. R 17.4.2.1(b)	
$A_{Nc0} = 9 h_{ef}^2$	ACI 318-14 Eq. (17.4.2.1c)
$\psi_{\text{ed,N}} = 0.7 + 0.3 \left( \frac{c_{\text{a,min}}}{1.5h_{\text{ef}}} \right) \le 1.0$	ACI 318-14 Eq. (17.4.2.5b)
$\psi_{cp,N} = MAX \left( \frac{c_{a,min}}{c_{ac}}, \frac{1.5h_{ef}}{c_{ac}} \right) \le 1.0$	ACI 318-14 Eq. (17.4.2.7b)
$N_b = k_c \lambda_a \sqrt{f_c} h_{ef}^{1.5}$	ACI 318-14 Eq. (17.4.2.2a)

#### Variables

h <sub>ef</sub> [in.]	c <sub>a,min</sub> [in.]	$\psi_{c,N}$	c <sub>ac</sub> [in.]	k <sub>c</sub>	λ <sub>a</sub>	f <sub>c</sub> [psi]
3.250	29.000	1.000	7.000	21	1.000	2,500

#### Calculations

A <sub>Nc</sub> [in. <sup>2</sup> ]	A <sub>Nc0</sub> [in. <sup>2</sup> ]	$\psi_{\text{ ed,N}}$	$\Psi_{\text{cp,N}}$	N <sub>b</sub> [kip]
95.06	95.06	1.000	1.000	6.152

N <sub>cb</sub> [kip]	♦ concrete	$\phi_{\sf seismic}$	$\phi_{nonductile}$	φ N <sub>cb</sub> [kip]	N <sub>ua</sub> [kip]
6.152	0.650	0.750	1.000	2.999	1.130





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## Fastening point:

### 4 Shear load

	Load V <sub>ua</sub> [kip]	Capacity $\Phi$ V <sub>n</sub> [kip]	Utilization $\beta_V = V_{ua}/\Phi V_n$	Status
Steel Strength*	0.940	8.034	12	OK
Steel failure (with lever arm)*	N/A	N/A	N/A	N/A
Pryout Strength**	0.940	8.613	11	OK
Concrete edge failure in direction y+**	0.940	11.716	9	OK

#### 4.1 Steel Strength

 $\begin{array}{lll} {\rm V_{sa,eq}} & = {\rm ESR~value} & {\rm refer~to~ICC\text{-}ES~ESR\text{-}4266} \\ {\rm \phi~V_{steel}} \geq {\rm V_{ua}} & {\rm ACI~318\text{-}14~Table~17.3.1.1} \end{array}$ 

#### **Variables**

A <sub>se</sub>	<sub>V</sub> [in. <sup>2</sup> ]	f <sub>uta</sub> [ksi]	$lpha_{ m V,seis}$
0	.16	114.604	1.000

#### Calculations

V<sub>sa,eq</sub> [kip] 12.360

V <sub>sa,eq</sub> [kip]	$\phi_{steel}$	$\phi_{nonductile}$	φ V <sub>sa,eq</sub> [kip]	V <sub>ua</sub> [kip]
12.360	0.650	1.000	8.034	0.940





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#### 4.2 Pryout Strength

$V_{cp} = k_{cp} \left[ \left( \frac{A_{Nc}}{A_{Nc0}} \right) \psi_{ed,N} \psi_{c,N} \psi_{cp,N} N_b \right]$	ACI 318-14 Eq. (17.5.3.1a)
$\phi V_{cp} \ge V_{ua}$	ACI 318-14 Table 17.3.1.1
A <sub>Nc</sub> see ACI 318-14, Section 17.4.2.1, Fig. R 17.4.2.1(b)	
$A_{Nc0} = 9 h_{ef}^2$	ACI 318-14 Eq. (17.4.2.1c)
$\psi_{\text{ed,N}} = 0.7 + 0.3 \left( \frac{c_{a,\text{min}}}{1.5h_{\text{ef}}} \right) \le 1.0$	ACI 318-14 Eq. (17.4.2.5b)
$\Psi_{\text{cp,N}} = \text{MAX}\left(\frac{c_{\text{a,min}}}{c_{\text{ac}}}, \frac{1.5h_{\text{ef}}}{c_{\text{ac}}}\right) \le 1.0$	ACI 318-14 Eq. (17.4.2.7b)
$N_b = k_c \lambda_a \sqrt{f_c} h_{ef}^{1.5}$	ACI 318-14 Eq. (17.4.2.2a)

#### Variables

К <sub>ср</sub>	h <sub>ef</sub> [ın.]	c <sub>a,min</sub> [ın.]	Ψ <sub>c,N</sub>	
2	3.250	29.000	1.000	
c <sub>ac</sub> [in.]	k <sub>c</sub>	λ <sub>a</sub>	f <sub>c</sub> [psi]	
 7.000	21	1.000	2,500	_

#### Calculations

A <sub>Nc</sub> [in. <sup>2</sup> ]	A <sub>Nc0</sub> [in. <sup>2</sup> ]	$\psi_{\text{ ed},N}$	$\psi_{\text{cp},\text{N}}$	N <sub>b</sub> [kip]
95.06	95.06	1.000	1.000	6.152

V <sub>cp</sub> [kip]	φ <sub>concrete</sub>	$\phi_{\sf seismic}$	$\phi_{nonductile}$	φ V <sub>cp</sub> [kip]	V <sub>ua</sub> [kip]
12.304	0.700	1.000	1.000	8.613	0.940





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#### 4.3 Concrete edge failure in direction y+

$V_{cb} = \left(\frac{A_{Vc}}{A_{Vc0}}\right) \psi_{ed,V} \psi_{c,V} \psi_{h,V} \psi_{parallel,V} V_{b}$	ACI 318-14 Eq. (17.5.2.1a)
$\phi V_{cb} \ge V_{ua}$	ACI 318-14 Table 17.3.1.1
A <sub>Vc</sub> see ACI 318-14, Section 17.5.2.1, Fig. R 17.5.2.1(b)	
$A_{Vc0} = 4.5 c_{a1}^2$	ACI 318-14 Eq. (17.5.2.1c)
$\Psi_{\text{ed,V}} = 0.7 + 0.3 \left( \frac{c_{a2}}{1.5c_{a1}} \right) \le 1.0$	ACI 318-14 Eq. (17.5.2.6b)
$\Psi_{h,V} = \sqrt{\frac{1.5c_{a1}}{h_a}} \ge 1.0$	ACI 318-14 Eq. (17.5.2.8)
$V_{b} = \left(7 \left(\frac{I_{e}}{d_{a}}\right)^{0.2} \sqrt{d_{a}}\right) \lambda_{a} \sqrt{\dot{f_{c}}} c_{a1}^{1.5}$	ACI 318-14 Eq. (17.5.2.2a)

#### Variables

c <sub>a1</sub> [in.]	c <sub>a2</sub> [in.]	$\Psi_{c,V}$	h <sub>a</sub> [in.]	l <sub>e</sub> [in.]	
29.000	29.000	1.000	6.000	3.250	
		2.2			
λ <sub>a</sub>	d <sub>a</sub> [in.]	f <sub>c</sub> [psi]	Ψ parallel,V		
1.000	0.625	2,500	1.000		

#### Calculations

$A_{Vc}$ [in. <sup>2</sup> ]	$A_{Vc0}$ [in. <sup>2</sup> ]	$\psi_{\text{ ed,V}}$	$\psi_{\text{h,V}}$	V <sub>b</sub> [kip]
435.00	3,784.50	0.900	2.693	60.090

#### Results

V <sub>cb</sub> [kip]	$\phi_{ m concrete}$	$\phi_{\sf seismic}$	$\phi_{nonductile}$	φ V <sub>cb</sub> [kip]	V <sub>ua</sub> [kip]
16.738	0.700	1.000	1.000	11.716	0.940

## 5 Combined tension and shear loads

$\beta_{N}$	$\beta_{V}$	ζ	Utilization $\beta_{N,V}$ [%]	Status	
0.377	0.117	5/3	23	OK	

$$\beta_{NV} = \beta_N^{\zeta} + \beta_V^{\zeta} \le 1$$





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#### 6 Warnings

- The anchor design methods in PROFIS Engineering require rigid anchor plates per current regulations (AS 5216:2021, ETAG 001/Annex C, EOTA TR029 etc.). This means load re-distribution on the anchors due to elastic deformations of the anchor plate are not considered the anchor plate is assumed to be sufficiently stiff, in order not to be deformed when subjected to the design loading. PROFIS Engineering calculates the minimum required anchor plate thickness with CBFEM to limit the stress of the anchor plate based on the assumptions explained above. The proof if the rigid anchor plate assumption is valid is not carried out by PROFIS Engineering. Input data and results must be checked for agreement with the existing conditions and for plausibility!
- Condition A applies where the potential concrete failure surfaces are crossed by supplementary reinforcement proportioned to tie the potential concrete failure prism into the structural member. Condition B applies where such supplementary reinforcement is not provided, or where pullout or pryout strength governs.
- · Refer to the manufacturer's product literature for cleaning and installation instructions.
- For additional information about ACI 318 strength design provisions, please go to https://submittals.us.hilti.com/PROFISAnchorDesignGuide/
- An anchor design approach for structures assigned to Seismic Design Category C, D, E or F is given in ACI 318-14, Chapter 17, Section 17.2.3.4.3 (a) that requires the governing design strength of an anchor or group of anchors be limited by ductile steel failure. If this is NOT the case, the connection design (tension) shall satisfy the provisions of Section 17.2.3.4.3 (b), Section 17.2.3.4.3 (c), or Section 17.2.3.4.3 (d). The connection design (shear) shall satisfy the provisions of Section 17.2.3.5.3 (a), Section 17.2.3.5.3 (b), or Section 17.2.3.5.3 (c).
- Section 17.2.3.4.3 (b) / Section 17.2.3.5.3 (a) require the attachment the anchors are connecting to the structure be designed to undergo ductile yielding at a load level corresponding to anchor forces no greater than the controlling design strength. Section 17.2.3.4.3 (c) / Section 17.2.3.5.3 (b) waive the ductility requirements and require the anchors to be designed for the maximum tension / shear that can be transmitted to the anchors by a non-yielding attachment. Section 17.2.3.4.3 (d) / Section 17.2.3.5.3 (c) waive the ductility requirements and require the design strength of the anchors to equal or exceed the maximum tension / shear obtained from design load combinations that include E, with E increased by ω<sub>0</sub>.
- Hilti post-installed anchors shall be installed in accordance with the Hilti Manufacturer's Printed Installation Instructions (MPII). Reference ACI 318-14, Section 17.8.1.

## Fastening meets the design criteria!



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#### 7 Installation data

Profile: no profile

Hole diameter in the fixture:  $d_f = 0.687$  in.

Plate thickness (input): 0.500 in.

Recommended plate thickness: not calculated

Drilling method: Hammer drilled

Cleaning: Manual cleaning of the drilled hole according to instructions for use is

required.

Anchor type and diameter: Kwik Bolt TZ2 - SS 304 5/8 (3

1/4) hnom2

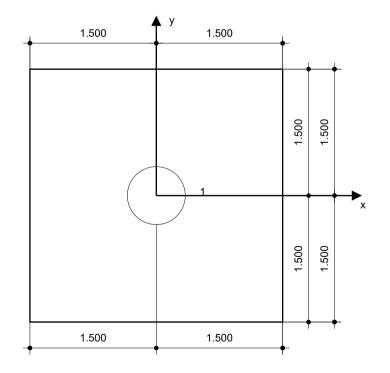
Item number: 2210279 KB-TZ2 5/8x6 SS304 Maximum installation torque: 0.06019 ft.kip Hole diameter in the base material: 0.625 in. Hole depth in the base material: 4.250 in.

Minimum thickness of the base material: 5.500 in.

Hilti KB-TZ2 stud anchor with 3.75 in embedment, 5/8 (3 1/4) hnom2, Stainless steel, installation per ESR-4266

#### 7.1 Recommended accessories

Drilling	Cleaning	Setting
Suitable Rotary Hammer	Manual blow-out pump	Torque controlled cordless impact tool
<ul> <li>Properly sized drill bit</li> </ul>		Torque wrench
		Hammer



## Coordinates Anchor [in.]

Anchor	x	у	C <sub>-x</sub>	C+x	C <sub>-y</sub>	C <sub>+y</sub>	
1	0.000	0.000	29.000	151.000	81.000	29.000	

Input data and results must be checked for conformity with the existing conditions and for plausibility! PROFIS Engineering ( c ) 2003-2022 Hilti AG, FL-9494 Schaan Hilti is a registered Trademark of Hilti AG, Schaan





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## 8 Remarks; Your Cooperation Duties

- Any and all information and data contained in the Software concern solely the use of Hilti products and are based on the principles, formulas and security regulations in accordance with Hilti's technical directions and operating, mounting and assembly instructions, etc., that must be strictly complied with by the user. All figures contained therein are average figures, and therefore use-specific tests are to be conducted prior to using the relevant Hilti product. The results of the calculations carried out by means of the Software are based essentially on the data you put in. Therefore, you bear the sole responsibility for the absence of errors, the completeness and the relevance of the data to be put in by you. Moreover, you bear sole responsibility for having the results of the calculation checked and cleared by an expert, particularly with regard to compliance with applicable norms and permits, prior to using them for your specific facility. The Software serves only as an aid to interpret norms and permits without any guarantee as to the absence of errors, the correctness and the relevance of the results or suitability for a specific application.
- You must take all necessary and reasonable steps to prevent or limit damage caused by the Software. In particular, you must arrange for the
  regular backup of programs and data and, if applicable, carry out the updates of the Software offered by Hilti on a regular basis. If you do not use
  the AutoUpdate function of the Software, you must ensure that you are using the current and thus up-to-date version of the Software in each
  case by carrying out manual updates via the Hilti Website. Hilti will not be liable for consequences, such as the recovery of lost or damaged data
  or programs, arising from a culpable breach of duty by you.



Form: Novato Fire Plan Review Form 2017-1 Master

## **Novato Fire Protection District**

Occupancy: Cingular Wireless PCS, LLC dba AT&T Mobility

Occupancy ID: 2413

Address: 150 Hamilton RD

Novato CA 94949

Inspection Type: 2 - Plan Review

Inspection Date: 9/28/2022 By: Osgood, Lynne (196)

Time In: 13:03 Time Out: 15:34

Authorized Date: 09/28/2022 By: Osgood, Lynne (196)

## **Inspection Description:**

Based on the 2016 California Building Standards Code, including the California Building and Fire Codes, along with current Novato Fire Protection District Standards.

## **Inspection Topics:**

## **Building Division Review**

Address Number Requirements.

The address shall be posted clearly visible from the street with numerals illuminated and contrasting color to their background conforming to Novato Fire Protection Standard #205.

Status: Condition of Approval

Notes:

Vegetation Management Plan - Fuels Management Plan Required.

An irrigated greenbelt Vegetation Management Plan (VMP) Fuels Management Plan conforming to the standards of the Novato Fire District shall be prepared and implemented at the site. The VMP-Fuels Management Plan shall conform to Novato Fire Protection Standard #220. The plan shall be incorporated into the landscape plan for the project and submitted to the Fire Marshal for review prior to implementation. The plan shall be implemented prior to building final.

Status: Condition of Approval

Notes:

NFPA 704 Placards Required.

NFPA 704 placards shall be installed conforming to Fire District Standard #309. The numerical ranking on the placards shall be in accordance with the highest hazard material as noted by the MSDS in each category as approved by the Fire Marshal.

Status: Condition of Approval

Notes:

Portable Fire Extinguishers Required.

Portable fire extinguishers shall be installed and maintained in accordance with California Fire Code Chapter 9.

Status: Condition of Approval

Notes:

### **Alternate Energy Supply Systems**

NFPA, California Fire Code, State Fire Marshal Building Standards and Regulations, Conformance Required.

Conformance required.

Status: Condition of Approval

Notes:

Novato Fire Protection District Standard Conformance Required.

This installation must be in conformance with Fire Protection District Standard #523.

**Status:** Condition of Approval

Notes:

#### Signage.

Signage shall be provided as required in Fire Protection District Standard #523 and the California Fire Code.

Status: Condition of Approval

**Notes:** Approved WARNING signage shall be provided and posted to warn emergency personnel that the power is backed up by a fuel fired generator. Shut down signage shall be provided

#### Final Inspection Required.

Final inspection of installed system including acceptance test is required.

Status: Condition of Approval

Notes:

#### Other Information.

See Below.

Status: Condition of Approval

**Notes:** Vehicle Impact Protection. 312.1 General vehicle impact protection required by this code shall be provided by posts that comply with Section 312.2 or by other approved physical barriers that comply with Section 312.3.

#### Placeholder

Х

Status: Condition of Approval

Notes:

Stationary generators. Stationary emergency and standby power generators required by the CFC code shall be listed in accordance with UL 2200.

Installation of stationary generators. Emergency power systems and standby power systems shall be installed in accordance with the California Building Code, the California Electrical Code, NFPA 110 and NFPA 111.

#### Letters

#### Plan Review Completion Report

Your plan submittal is complete for the subject project and is subject to the conditions and notes indicated. You are required to contact the Novato Fire Protection District for all noted inspections at least 48 hours in advance. We are returning plans that have been reviewed. The Fire District will retain one set for our files. A reviewed stamped set of plans must be maintained on the project site for reference by District Inspectors at all times. To schedule appointments for inspections and tests, contact the Fire District Administrative Office at (415) 878-2690 during business hours and at least 48 hours in advance of the required inspection. Should you have any questions about your project please contact me or the Fire Marshal at (415) 878-2620. Thank you.

**Status:** Condition of Approval

Notes:

## **Additional Time Spent on Inspection:**

Category Start Date / Time End Date / Time

Notes: No Additional time recorded

Total Additional Time: 0 minutes Inspection Time: 151 minutes

**Total Time: 151 minutes** 

## Summary:

Overall Result: Plan Review - Complete

**Inspector Notes:** 

Inspector:	
Name: Osgood, Lynne Rank: Deputy Fire Marshal	

## CITY OF NOVATO

# WASTE MANAGEMENT PLAN (WMP) FOR CONSTRUCTION DEMOLITION (C&D) RECYCLING AND REUSE



Small Projects, as defined on Page 2. (Fill out Parts 1 & 2)

Using Recology Sonoma-Marin\* Debris Box?

**Yes** (Fill out part 1 only)

No (Fill out Part 1 now & Part 3 at Final)

\*Note- Recology Sonoma-Marin is the designated provider for debris box services within the City of Novato.

Part 1: Project Overview
Job Address Permit Number
Owner Contractor
Owner's Phone Number Contractor's Phone Number
Waste Hauler or Recycling Contractor Phone Number
Part 2: Small Projects
The above checked building component being replaced shall be recycled or reused in accordance with Novato Municipal Code Section 4-12.
Part 3: Material Generation and Recycling – Complete for FINAL  1. Total volume or weight of construction or demolition debris, by type:  Construction Actual Final Weight  Demolition Actual Final Weight
Volume or weight or description of materials that can feasibly be diverted via reuse:     Actual Final Weight  Description of materials for reuse
3. Facility/Facilities receiving materials:
4. Final Inspection Requirements:  →Receipt from waste hauler or recycling contractor  →Redwood Landfill receipts MUST have their Recyclable C&D stamp for acceptance by City of Novato  →Waste Management Plan Form submitted with required receipts  →Exception: Part 2 permit types with signed penalty of perjury statement
PENALTY OF PERJURY STATEMENT  I declare under penalty of perjury, under the laws of the State of California, that all statements contained in this application are true and correct, with full knowledge that all statements made in this application are subject to investigation and that any false or dishonest answer to any question may be grounds for revocation of the building permit.
Signed:         Owner         Contractor         Date:
FINAL APPROVAL

Inspector

Date

# CITY OF NOVATO CONSTRUCTION & DEMOLITION WASTE RECOVERY ORDINANCE INFORMATION BULLETIN

#### **Community Development Department, Building Division**

Many of the materials generated from your project can be successfully diverted from the landfill through recycling or reuse. You are required to recycle or reuse at least 50% of these materials. The building official may impose a fine for failure to comply with this condition.

**COVERED PROJECTS:** Every construction, demolition, and renovation project within the City of Novato.

<u>SMALL PROJECT permits</u>, such as minor plumbing upgrades or electrical service upgrades, additional circuits/receptacles/light fixtures or mechanical residential ventilation fans, fireplace inserts or building - add skylight, repair exterior siding. Compliance to be by completion of the Penalty of Perjury Statement.

ROOFING CONTRACTORS: Compliance to be by completion of the Penalty of Perjury Statement and periodic requests for receipts from approved recycling facility.

Replacement of HVAC, water heater or windows. Compliance to be by completion of the Penalty of Perjury Statement.

The goal is to divert, by recycling or reuse, 50% or more of the scrap materials (by weight) from the project. A waste management plan (WMP) must be completed before your construction or demolition permit will be issued.

## COMPLIANCE BY USE OF WASTE HAULER

Submittal of receipts from State licensed recycling/reuse facilities (see list below) or waste hauler who takes materials to these facilities is required for compliance. Compliance is required as a condition of approval for a building permit and for final approval and/or occupancy of the building.

## **COMPLIANCE BY SELF HAULER**

Collect and attach all receipts or reports for disposal and recycling from State licensed facility. In Part 3 of this document fill in the actual disposal and diverted weight for each material. Using the actual weights, calculate the diversion rate for your final submittal.

ris	ris Bo	ris Boxes:

1. Recology Sonoma-Marin	800-243-0291
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#### **Self Haulers:**

# RECEIPTS WILL BE ACCEPTED FROM THESE APPROVED RECYCLING OR REUSE FACILITIES:

1. Redwood Land Fill\* 8950 Redwood Highway, Novato, CA 415-892-2851

2. Marin Resource Recovery Center Public Dump, 565 Jacoby Street, San Rafael, CA 415-485-5646

3. Global Materials Recovery Service 3911 Santa Rosa Avenue, Santa Rosa, CA 707-585-0511

<sup>\*</sup> Redwood Landfill receipts MUST have their Recyclable C&D stamp to be accepted by the City of Novato.